

NATIONAL STEEL BRIDGE ALLIANCE

AASHTO/NSBA Steel Bridge Collaboration

Fall Meeting Minutes - Combined

Little Rock, AR

October 21 – 23



The AASHTO/NSBA Steel Bridge Collaboration is a joint effort between the American Association of State Highway and Transportation Officials (AASHTO) and the National Steel Bridge Alliance (NSBA) with representatives from state departments of transportation, the Federal Highway Administration, academia, and various industry groups related to steel bridge design, fabrication, and inspection. The mission of the Collaboration is to provide a forum where professionals can work together to improve and achieve the quality and value of steel bridges through standardization of design, fabrication, and erection.

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Task Group List

Group Name	Chair	Chair Company	Vice Chair	Vice Chair Company
TG 1 Detailing	Randy Harrison	W&W AFCO Steel	Gary Wisch	DeLong's, Inc.
TG 2 Fabrication and Repair	Heather Gilmer	Pennoni	Duncan Paterson	NSBA
TG 4 QC/QA	Jamie Hilton	KTA-Tator, Inc.	Robin Dunlap	High Steel Structures
TG 8 Corrosion Protection	Johnnie Miller	KTA-Tator, Inc.	Derrick Castle	Sherwin-Williams
TG 9 Bearings	Michael Culmo	CHA Consulting, Inc.	Ron Watson	RJ Watson, Inc.
TG 10 Erection	Brian Witte	Parsons	Jason Stith	Michael Baker International
TG 11 Design	Brandon Chavel	NSBA	Domenic Coletti	HDR
TG 12 Design for Constructability and Fabrication	Russell Jeck	GZA GeoEnvironmental Inc.		
TG 13 Analysis of Steel Bridges	Deanna Nevling	HDR	Francesco Russo	Russo Structural Services
TG 14 Field Repairs and Retrofits	Kyle Smith	GPI	Nick Haltvick	Minnesota Department of Transportation
TG 15 Data Modeling for Interoperability	Aaron Costin	University of Florida	Grant Schmitz	HDR
TG 16 Orthotropic Deck Panels	Sougata Roy	SOCOTEC Engineering, Inc.	Frank Artmont	Modjeski & Masters, Inc.
TG 17 Steel Castings	Jennifer Pazdon	Cast Connex	Jason Stith	Michael Baker International
TG 18 Duplex Stainless Steel	Jason Provines	Virginia Department of Transportation	Nancy Baddoo	Steel Construction Institute
TG 19 Movable Bridge	George Patton	Hardesty & Hanover, LLC	Frank Artmont	Modjeski & Masters, Inc.
Main Committee	Ronnie Medlock	High Steel Structures	Natalie McCombs	HNTB

Past Meeting Notes

Year	Meeting	Link
2018	Spring	Not Available
	Fall	Meeting Notes
2019	Spring	Meeting Notes
	Fall	Meeting Notes
2020	Spring	Meeting Notes
	Fall	Meeting Notes
2021	Spring	Meeting Notes
	Fall	Meeting Notes
2022	Spring	Meeting Notes
	Fall	Meeting Notes
2023	Spring	Meeting Notes
	Fall	Meeting Notes
2024	Spring	Meeting Notes
	Fall	Meeting Notes
2025	Spring	Meeting Notes
	Fall	This Document

Current Meeting Notes



AASHTO/NSBA Steel Bridge Collaboration

TG 1 Detailing

Embassy Suites

Little Rock

Room Name: Rock Island 3

Task Group Mission: This Task Group is specifically responsible for the creation and maintenance of guidelines and best practices for the creation of clear concise design and fabrication drawings.

Task Group Leadership

Chair: Randy Harrison - W&W|AFCO Steel

Vice Chair: Gary Wisch - DeLong's, Inc.

Meeting Agenda: 10/22/2025 (3:00 PM - 5:00 PM CT)

1. Chairperson's Welcome (3:00 PM – 3:10 PM)
 - a. AISC Antitrust Policy and Meeting Code of Conduct.
 - b. Introductions (as needed).
 - c. [Approval of Previous Meeting Minutes.](#)
2. G1.1 Approval Requirements (3:10 PM – 4:00 PM)
 - a. Review of responsibilities of fabricators vs checkers/owners reviewers
 - b. Review of comments for Section 4:
 - c. 8 voted in favor in simplifying/streamline document // To be reviewed by group outside of this meeting (Due Date: 1/31/2026)
 - i. Brad Dillman to review A,B&C
 - ii. Randy Harrison to review E&F
 - iii. Gary Wisch to review G,H & I
 - iv. Bill Laley to review J,K,L
 - v. Brian to review M,NO
 - vi. Entire document to be reviewed by Dom Coletti & Eric Rau
 - d. Reference to Iowa DOT Review Checklist
3. G1.3 & G1.4 Combined drawings and review requested by TG (4:00 PM – 5:00 PM)
 - a. Reviewed previous comments and addressed new suggestions

- b. Page 2, Remove “Expect that stiffeners, intermediate and end crossframes and lateral bracing may be Grade 36”
 - c. Page 2, Remove that fabricator must have Fracture Critical endorsement and replace with current wording
 - d. Look at separating engineer instructions from examples and comments.
 - e. Provide notes that are only required to be included, remove “example notes” and keep “notes for designer” ...GUIDELINE FOR DRAWINGS (Randy)
 - f. Add General Note: Specify Material Grade, Bolt Grade
 - g. Remove Note under Steel Fabrication: “Fabricator of structural steel shall have the appropriate AISC Quality Certification”
 - h. Charpy V-Notch Note: Designer should specify Charpy- V Notch testing and specify which members
 - i. Small task group to review what is required for General Notes Section
 - i. Brad, Bill L, Heather, Jessica W, Eric R and Randy to meet week of December 8
 - j. Girder Elevation Sheet – Remove Tension Flange Connection Detail
 - k. Connection Plate (Stiffener) vs Transverse Stiffener
 - i. No Option 1 on Curved Girders
 - l. Standard Clip & Weld Termination Detail to be revised
4. Adjourn



AASHTO/NSBA Steel Bridge Collaboration

TG 2 Fabrication and Repair

Embassy Suites

Little Rock

Room Name: Rock Island 4-7

Task Group Mission: This Task Group aims to achieve quality and value in the fabrication of steel bridges through standardization of steel bridge fabrication across the nation.

Task Group Leadership

Chair: Heather Gilmer - Pennoni

Vice Chair: Duncan Paterson - NSBA

Meeting Agenda: 10/21/2025 (9:00 AM - Noon CT)

1. Chairperson's Welcome (9:00 AM – 9:10 AM)
 - a. AISC Antitrust Policy and Meeting Code of Conduct.
 - b. Introductions (as needed).

Add Dallas Stevens, David Perez, Chris Livsey, and Daniel Trotta of ARDOT and Kay Jimison of Valmont as in attendance. They were not connected to the Zoom.

Following introductions, Heather provided an overview of the documents that are directly and indirectly under the guidance of this Task Group.

- c. [Approval of Previous Meeting Minutes.](#)

No discussion. Meetings minutes approved.

2. 2.AASHTO fabrication specification
 - a. Check assemblies (Gilmer, Medlock, Patton)

AASHTO Steel Bridge Fabrication Specification, Article 17.5.3

- A ballot was previously proposed to revise Article 17.5.3 and its commentary; however, several AASHTO comments expressed concerns with the proposed changes.
- The key issue is ensuring that owners retain the ability to require additional check assemblies when they deem necessary.

- Background and Discussion Points
- Comments were received from the Steel and Metals Technical Committee as well as the Committee on Bridges and Structures (COBS).
- Some provisions from the AASHTO Construction Specification have been relocated to the Fabrication Specification.
- The existing commentary suggested that inspectors could request a check assembly at any time—essentially at the owner’s discretion.
- The draft revision introduced a provision allowing use of CNC fabrication in conjunction with limited check assemblies (used to verify fit prior to full production). Once fit was verified, subsequent assemblies were deemed unnecessary.

Owner Concerns

- During a call with the Steel and Metals Committee, several owners stated that the proposed language limited their ability to request additional assemblies as needed.
- The original assumption was that additional check assemblies would only be required if fit-up issues occurred; however, owners want the flexibility to specify additional assemblies in their own project or standard specifications.
- Owners also emphasized the importance of standardization across states, while maintaining the ability to state deviations clearly when needed.
- Clarifications and Recommendations
- Some owners feel that recent revisions to the Fabrication Specification may reduce owner control over certain aspects they previously managed. This was not the intent—the intent was only to address the possibility of “spur-of-the-moment” check assembly requests.

- Ronnie Medlock recommended clarifying in the specification that owners may include additional requirements in their own standard specifications (for example, requiring more assemblies than the minimum stated).
- It was agreed that the Fabrication Specification is not intended to serve as a consolidation of all state requirements, but rather to establish a baseline that states can build upon.
- Heather recommended adding this as a new business item focused on alternative methods, with interim acknowledgment in the commentary.
- It may be sufficient to provide GDOT with an explanation of the task group's direction rather than revising the specification language at this time.
- Alina Davidescu made a point to consider minimum versus overruling.
- Heather suggested adding "at least" language to the specification. Or "one or more". The attendee preferred "one or more". Owner specifies how many or if the owner does not specify, the fabricator can choose to take into consideration the possibilities of back charges should there be fit issues in the field.

Other Business

- Karl Frank suggested that virtual assembly should eventually be incorporated into the specification.
- Ronnie Medlock suggested that there be some mention of cross-frame assembly and fit. Right now, the specification excludes cross-frames from check assemblies.
- Heather suggested that the existing NSBA "Fit Document" be reviewed and updated as necessary.
- NCHRP synthesis collected information on state preferences for tolerances and erection. It was recommended that the task group review the synthesis and update the fabrication specification as necessary.

NCHRP Synthesis 603 — Practices for Steel Bridge Fabrication and
Erection Tolerances (2023).

- b. Scribing/etching of layout marks (Diarcangelo, Medlock, Michalk, McCullough, Wiersh)

Piece Marking of Steel During Fabrication

- Discussion focused on the use of plasma for marking layout lines, in contrast to deeper piece marks and match marks.
- Consensus from previous meetings remains that specification language is not practical or necessary, but that a commentary section on workmanship should be developed to provide guidance.

Current Specification Context

- The existing document already contains provisions related to piece marking, low-stress markings, and other identification methods; however, these sections could benefit from consolidation and clarification.
- There is currently no specific language addressing layout marks, particularly in relation to modern CNC fabrication practices.

Workmanship and Preservation of Marks

- Heather proposed including commentary language addressing workmanship requirements for different marking methods and reviewed preliminary draft text with the group.
- Additional commentary may be needed regarding the maintenance and preservation of marks through subsequent fabrication and coating processes.
- Current language indicates that marks should remain legible after coating; the group discussed whether this requirement should be strengthened with “shall” language.

- Consideration should also be given to offsite coating processes, such as galvanizing, to ensure marking visibility and orientation are maintained.

Future Topics

- Match mark orientation and related layout practices were identified as potential new business items for future discussion.
- Language related to the depth of the mark as it relates to marks that are overly deep should be considered. Differentiate between match marks that need to be visible throughout each step versus those that only need to be temporarily visible.
- Karl Frank said if you can compare the depth to the allowable for undercut. If you are not any deeper than the undercut limit or surface roughness might be a way to measure depth of a mark (i.e., validation of the depth).
- Add reference to Florida DOT marking study in the absence of specific guidance.
- Ronnie Medlock suggested that the equipment manufacturers perform some type of study or provide information related depth and consistency.
- Task group will table the topic for now. The task group should consider writing a research needs statement that would provide answers to the questions so that they may be better able to make recommendations.

TODO: Include attachment from Heather.

3. G2.2 - Guidelines for Resolution of Steel Bridge Fabrication Errors

The G2.2 document was originally developed to capture and preserve industry knowledge that might otherwise be lost as experienced personnel retire or leave the field. Its purpose is to document best practices and lessons learned to ensure that critical expertise is passed down to the next generation.

Next Steps

- Future updates should include input from fabricators and bridge owners, particularly regarding nonconformance reports (NCRs) or issues that may not currently be addressed in the existing guidelines.
- It was suggested that this effort could be initiated through the Fabrication Task Force within the AASHTO Steel and Metals Technical Committee, which would provide a structured channel for gathering feedback and proposed additions.

Future Topics

- Look for synergies with the G14.3 repairs database. Also consider how the recommendations in the G2.2 are affected by field application.
- a. Improper preheat (Medlock, Gramlick, Niemann, Frank, Ocel, Provines, Roy)

The concerns associated with improper preheat are porosity or cracking due to the presence of high hydrogen and high heat affected zone (HAZ) hardness due to rapid cooling. Therefore, the recommended remedy is as follows:

- Do a visual inspection
 - Conduct MT
 - For CJP groove welds, conduct UT
 - Commentary: Check the HAZ hardness of the suspect area
 - Compare with PQR hardness results if they are available, or
 - Compare with similar areas that were properly preheated
- b. Framing members too short (Paterson, Rau, Dillman, Elsayed, Svatora)

Duncan Paterson created several sketches. Next steps would be to write descriptions for the images.

TODO: Include attachment from Heather.

- c. Elements of rolled beams not aligning at a splice—or built-up members after applying depth tolerance (Wisch, Leonard)

Recall that the underlying goal is to provide guidance for something that should be simple but require an NCR and there is a possibility of design differences resulting from the addition of the filler plate. Application of correctio can apply to built-up plate girders, however it is less frequent.

TODO: Include attachment on repair recommendations from Heather.

- d. General Updates for D1.5 changes, AASHTO Fab Spec, FC terminology, etc. (Gilmer)

We will continue to go over comments as time permits. If you want a preview, check out the bold comments in the draft, particularly starting at section 2.4, middle of case 3. Draft is here:

<https://docs.google.com/document/d/1GTjsJ1HRHNnZSbgM6rKQihy1a1vJ0PYE/edit?usp=sharing&ouid=101686789017403472572&rtpof=true&sd=true>

Specific action items from prior discussion:

- Do we have anyone who can redraw figures that need redrawing? The mislocated hole figures in particular probably need help. High Steel volunteered to redraw figures.
- 2.2: This sentence was moved from “recommendation” to “commentary”, but do we need it at all? Does anyone in our audience not know what a free edge is?
- A “free edge” is a rolled or thermally cut boundary not welded to another component. This includes the end or side edges of a flange, the end of a web, or any edge of a splice plate.

Consider a similar approach in the general notes to concrete cover. For example, not allowing less, however more may be alright.

- 2.2The solution of neglecting the whole row and just adding a new one is in the figure, but there is no recommendation to do this.

- 2.4: Add subcase where the dimension of the hole is NOT within AASHTO oversize definition. Eric Rau and Geoff Swett volunteered.

4. Adjourn



AASHTO/NSBA Steel Bridge Collaboration

TG 4 QC/QA

Embassy Suites

Little Rock

Room Name: Rock Island 3

Task Group Mission: This task Group primarily focuses on the requirements for a Fabricator's quality control program, with emphasis on the development and implementation of a quality control plan and minimum requirements for an Owner's quality assurance program. At the same time the group acknowledges the need for a cooperative approach to quality, where the Owner's and Contractor's representatives work together to meet their responsibilities, resulting in the efficient fabrication of steel bridges meeting all contractual requirements.

Task Group Leadership

Chair: Jamie Hilton - KTA-Tator, Inc.

Vice Chair: Robin Dunlap - High Steel Structures

Meeting Agenda: 10/22/2025 (8:00 AM - Noon CT)

1. Chairperson's Welcome (8:00 AM – 8:10 AM)
 - a. [AISC Antitrust Policy and Meeting Code of Conduct.](#)
 - b. Introductions (as needed).

New members Charlies and Jose to committee.
 - c. [Approval of Previous Meeting Minutes.](#)
2. G4.1 - Steel Bridge Fabrication QA/QC Guidelines (8:10 AM – 8:20 AM) - Status update:
ready for publication.

Document has completed typesetting and is awaiting a final cover which is being created by AASHTO Pubs group. Once that is done, the final document will receive a quick review and then be posted for download on both the NSBA and AASHTO websites.

3. S4.3 – Specification for Owners Inspection and Inspectors (8:20 AM – 11:30 AM)

Background

- The S4.3 Specification was balloted about a year ago, and many comments have already been addressed in previous meetings.

- The document originated from an older specification, which was restructured and refined to improve clarity, flow, and accuracy.
- The intent is to develop it as a standalone specification so that owners can incorporate it directly into their standard specifications for use with third-party inspectors.
- This meeting continued review of remaining TG ballot comments, building on progress from the Spring 2024 meeting.

Document Revisions and Status

- Table 3-1 will be corrected to ensure the required years of experience align with AISC requirements.
- Redundant sections are being consolidated where appropriate, without altering technical meaning.
- More than 60 comments remain unresolved and will continue to be reviewed in future meetings.

Discussion on Terminology and Definitions

- Heather Gilmer’s comment on Section 5.5 raised questions about the use of “verify” and “monitor.”
 - Both actions occur during inspection and are generally used appropriately.
 - However, the comment prompted a broader review for consistency and clarity, since these terms describe distinct inspection activities that could be misinterpreted in shop practice.
- The group agreed to also review terms like “inspection” for consistency throughout the document.
- Some of these actions result in specific work products (e.g., reports or checklists).
- The group recommended expanding the definitions section to include these terms and describe what each typically involves.

Recommendations and References

- Robin Dunlap suggested adding “notify” to the definitions list.

- Terry Logan noted that definitions for similar terms appear in ASQ documents and recommended using those as reference sources rather than creating entirely new definitions.
- Jamie observed that prior versions of this document sometimes developed their own terms but generally sought alignment with AISC terminology.
- Art Bustos mentioned that relevant definitions may be found in the AISC Code of Standard Practice, AISC 360, and AISC 270.
- Terry Logan emphasized selecting a single primary standard as the basis for definitions to avoid conflicts in interpretation or arbitration.
- Jamie proposed a structured review process:
 - Compare definitions with AISC first.
 - If not defined there, default to ASQ or another reputable source.
- Heather Gilmer added that any new definitions developed for S4.3 that do not appear elsewhere (e.g., in the AASHTO Fabrication Specification) should also be shared or pushed to those related documents.

Action Items

- Ronnie Medlock will help develop new and revised definitions, coordinating with staff at High Steel.
- Phil Sauser and Art Bustos will review existing definitions for consistency with AISC and ASQ terminology.
- If a term is not found in either reference, the current language will remain.

Discussion of Specific Sections

Sections 5.6.2 and 5.6.3 – NCR Submissions

- Heather’s comment: “Review and confirm the Fabricator’s proposed methods of repair and description of the existing material condition” appears twice (once in each section).
- The group discussed whether the more detailed version in 5.6.3 should replace the shorter one in 5.6.2.

- Heather suggested instead adapting Section 5.6.2 as commentary to accompany Section 5.6.3.
- Jamie recommended that both sections be reviewed and revised for consistency.
 - TODO: Heather Gilmer and Robin Dunlap will review these sections and suggest updates to address the original comment.

Section 6.3 – Owner Permission

- Review of Heather’s related comment was deferred to a future meeting.

Section 7.2.1

- TODO: Heather will review this section and propose revised wording.

Section 7.2.3 – Signoff on MTRs (Mill Test Reports)

- Discussion focused on timing of MTR submission.
- In some cases, MTRs are provided after fabrication begins, particularly when work is staged.
- Ronnie expressed concern with the phrase “prior to start” under these conditions.
- Jamie proposed simplifying the text to:

*“The Owner’s Inspector shall...”
followed by the list of required actions.*

- Heather recommended shortening the second bullet, but Terry cautioned against removing too much detail.
- Ronnie reminded the group that the document should reflect best practices, not state-specific procedures.
- The group agreed to remove the second half of the sentence and move additional context to the commentary section.
 - TODO: Jamie, Matt and Tereasa Michalk will assist with these edits.

Section 7.2.3 – Identifying Mark Placement

- Decision: move this bullet from mandatory text to commentary.

Section 7.2.3 – Buy America Commentary

- Decision: delete the commentary regarding Buy America and remove reference to aluminum, as it was deemed unnecessary.

Section 7.2.9 – Distribution of MTRs

- Decision: revise to include “Owner or Owner’s Inspector” to cover both possibilities for submittal.

Section 7.6.2.1 – Radiographic Testing (RT)

- Heather raised whether recommendations in this section were directed toward fabricators rather than inspectors.
- The group confirmed that S4.3 is written for inspectors.
- Terry noted this topic is covered elsewhere and, if retained here, should appear in commentary form with generalized language.
- The group also discussed that many inspectors do not witness RT firsthand, since it is often completed before their arrival.
- A suggestion was made to include conditional language such as “if witnessing” where applicable.
 - TODO: Jamie and Phil Saucer to edit.

Section 7.7 – Fastener Testing

- The group recommended expanding this section and commentary to include distributor testing and related cases.
 - It was noted that some Owners require independent sampling and testing of fasteners.
 - TODO: Art Bustos will investigate and propose commentary additions.
4. G4.2 – Guidelines for the Qualifications of Structural Bolting Inspectors – (11:30 AM - 11:50 AM) start addressing new business from the AASHTO COBS ballot comments.

Review of Previous COBS Comments

- Jamie led the discussion of comments received during the previous COBS review. A recurring point of confusion among reviewers was the document’s use of “should”

and “shall.” Several comments reflected uncertainty about whether the document was intended to function as a formal specification or as guidance. The group clarified that while the document has a specification-like structure, its purpose is to serve primarily as guidance.

- Some state DOTs prefer a degree of flexibility rather than prescriptive requirements, and the document’s organization accommodates that approach. Ronnie Medlock suggested that commentary sections could be expanded to provide additional technical detail or examples, thereby satisfying agencies seeking more explicit direction without changing the main body of the text.

Section 3.3 – Experience Requirements

- The group discussed the experience requirements in Section 3.3, focusing on who is authorized to certify experience and whether such certification should have an expiration date. The consensus was that no expiration period should be imposed.

Section 4.1 – Requalification and Retesting

- The group reviewed Section 4.1 and agreed that inspectors who perform their work regularly should not be required to undergo periodic retesting. The intent is to avoid imposing requirements similar to those applied to welders, since this document applies specifically to inspectors. The section was revised to clarify these points and provide additional explanation of qualification expectations. These updates address comments submitted by Doug Cantrell (NYSDOT).

Section 5.4.3.1 – Determining Gaps

- The group agreed that a PIV (Pre-Installation Verification) test is not necessary for determining gaps. Accordingly, the related language will be removed. The commenter had referenced “Appendix A” without specifying a document; the group determined this likely referred to an older edition of S10.1. The corresponding sections no longer exist in the current edition. This comment was submitted by James Corney (Utah DOT).

Section 5.4.3.2 – Snugging

- Since PIV testing is no longer performed for DTIs, the comment related to snugging is no longer applicable. (Comment from James Corney, Utah DOT.)

Section 5.4.3.3 – Avoiding Redundant Requirements

- The group agreed that the document should not repeat existing requirements; therefore, no action will be taken in response to this comment. (Comment from James Corney, Utah DOT.)

Other Discussion

- It was noted that bolt installer qualification and training requirements are now covered under the updated RCSC Specification. The group agreed to wait for the next edition of RCSC to be published before considering any further changes related to these provisions. This would include adding the “combined method” to the Body of Knowledge. Should also consider adding a reference to the AASHTO LRFD Steel Bridge Fabrication Specifications Annex A – Common Provisions for Bolted Connections.

5. New Business/General open discussion (11:50 AM – Noon)

Next Steps and Coordination

- A virtual meeting will be scheduled to discuss remaining S4.3 comments once several of the assigned action items have been completed. Chris will provide periodic reminders to Jamie to help coordinate this session.
- The group discussed reestablishing a joint meeting with other Task Groups to address guidance related to bolting installer qualifications. It was noted that RCSC has developed training videos covering these topics, which are currently in post-production editing.
- Terry Logan cautioned against introducing overly prescriptive requirements and questioned whether a formal document specific to bolt installers is necessary within this group’s scope.

6. Adjourn



AASHTO/NSBA Steel Bridge Collaboration

TG 8 Corrosion Protection

Embassy Suites

Little Rock

Room Name: Rock Island 3

Task Group Mission: This Task Group primarily focuses on the functions, operations, requirements and activities needed to achieve consistent quality in steel bridge corrosion protection systems. At the same time the group acknowledges the need for a cooperative approach to quality, where the Owner's and Contractor's representatives work together to meet their responsibilities, resulting in efficient steel bridges coatings that meeting all contractual requirements.

Task Group Leadership

Chair: Johnnie Miller - KTA-Tator, Inc.

Vice Chair: Derrick Castle - Sherwin Williams

Meeting Summary: 10/22/2025 (1:00 PM - 3:00 PM CT)

1. Chairperson's Welcome (1:00 PM – 1:10 PM)
 - a. [Approval of Previous Meeting Minutes.](#)
2. Update of S8.1 document (1:10 PM – 1:15 PM)
 - a. Chris provided a quick recap of the document balloting process. The document has been presented at AASHTO Steel and metals and is in their hands. Heather added that it was balloted through AMPP.
 - b. Chris provided an update on the baseline testing that is underway with KTA Tator
3. Review S8.2 (1:15 PM – 1:45 PM)
 - a. Jeff and Heather Gilmer went through the major changes to S8.2 and any significant changes are noted in the google document which will be reflected in the version that goes to ballot with TG8.
 - b. A task group was formed to investigate and recommend changes to the document related to the bend test that Geoff Swett brought up. Jeff will organize a virtual meeting to discuss. The group consists of: Brad Dillman, Heather Gilmer, Brad Streeter, Kara Lorenz, Geoff Swett, Jason Stalnaker, and Teresa Michalk.
 - c. After resolution is found related to the bend test discussion, a version of the proposed changes will be sent out for ballot to TG8 via specbuilder.

4. Review G8.4 (1:45 PM – 2:20 PM)

- a. Derrick provided an update from Alana Fossa regarding the progress of G8.4.
 - i. UWS/50CR (Oct 1): met to discuss the overlap with UWS reference guide.
Overall this section is going to refer to the NSBA Reference guide for Uncoated Weathering Steel. Jeff introduced the suggestion that Jennifer McConnell had about adding a general section to cover general recommendations for all bridge regardless of coatings. Ronnie, and the group, agreed that this is a good idea.
 - ii. TSZ (Oct 3): trying to work around the status of CS-23 and S8.2. Will use the 2019 draft of CS-23, and latest draft of S8.2 as their references. Group will begin meeting monthly (Nov 12 next), and will focus only on items that are metallizing specific (avoid overlap with liquid coatings sections, except as noted).
 - iii. Liquid Applied Coating (n/a): did not meet due to an issue with teams meeting (likely an issue on my end). Need to reschedule, but they are set with an agenda, etc.
 - iv. HDG (Sept 29): document is in good shape, but it took us most of the meeting just to catch up on where the group left off. We are mostly gathering additional images and figured out how to clean up the comments we had already addressed or have since been addressed in S8.3. At our next meeting in Nov 20, we will start working through any final (but relatively few) remaining comments.

5. Update of Uncoated Weathering Steel guide - Tom Murphy (2:20 PM – 2:50 PM)

- a. Tom provided an update with a ppt. This document is going to be absorbed by TG8 as the FHWA will not be updating the FHWA Technical Advisory.

6. Open Discussion(2:50 PM – 3:00 PM)

- a. Jeff shared the updated relative cost of corrosion protection survey
- b. Randy Harrison asked if anyone had been instructed not to install studs prior to galvanizing, and whether alternatives were provided to prevent galvanizing of the top flange or if grinding was required to install the studs.

7. Adjourn



AASHTO/NSBA Steel Bridge Collaboration

TG 9 Bearings

Embassy Suites

Little Rock

Room Name: Rock Island 3

Task Group Mission: This Task Group is specifically responsible for the creation and maintenance of guidelines and best practices for steel bridge bearings.

Task Group Leadership

Chair: Michael Culmo - CHA Consulting, Inc.

Vice Chair: Ron Watson - RJ Watson, Inc.

Meeting Summary: 10/23/2025 (8:00 AM - 10:00 AM CT)

1. Chairperson's Welcome (8:00 AM – 8:10 AM)
 - a. [Approval of Previous Meeting Minutes.](#)
2. Old Business (8:10 AM - 9:30 AM)
 - a. Discussion on draft provisions for bearing maintenance.
 - i. Mike summarized the intent of the new document and that it will be a new chapter to be added into G9.1.
 - ii. Mike reviewed the current table of contents with the group.
 - iii. Mike skimmed through the document to give the group an idea of what is included in the document.
 - iv. He asked for volunteers to write various sections of the new document and he took notes on volunteers directly in the document.
 - v. Brian Atkinson volunteered to review the FHWA training for bridge bearing inspection and see if there is anything in that training that could fit into this section.
 - vi. Target May 2027 to get the first draft to Chris for Collaboration balloting. Then sent to AASHTO by September 2027.
 - vii. Mike is requesting that the initial writing assignments are done and sent to him by end of February 2026.
 - b. Discussion on draft document for large movement deck expansion joints

- i. Mike reviewed the purpose for this document and what is planned to be included in the document.
 - ii. He went through the table of contents and discussed with the group about what is to be included in the document.
 - iii. Mike asked the group if we are biting off too much to be working on both documents. Ron didn't think that it we were doing too much and should continue.
 - iv. Mike asked for volunteers to write certain sections and took notes directly in the document.
 - v. Target May 2027 to get the first draft to Chris for Collaboration balloting. Then sent to AASHTO by September 2027.
 - vi. Mike is requesting that the initial writing assignments are done and sent to him by end of February 2026.
- c. Mike is requesting that everyone who is writing sections for both documents should email him the text so he can maintain the proper formatting of the word document.
 - d. He would like to use Bluebeam for reviewing the document and he will add everyone who is currently writing/reviewing to a new bluebeam session.
3. Adjourn



AASHTO/NSBA Steel Bridge Collaboration

TG 10 Erection

Embassy Suites

Little Rock

Room Name: Rock Island 4-7

Task Group Mission: This Task Group develops guidelines and specifications that establish and define the basic, minimum requirements for the transportation, handling and erection of steel bridge components to ensure safe steel erection as well as quality and value in the completed bridge structure.

Task Group Leadership

Chair: Brian Witte - Parsons

Vice Chair: Jason Stith - Michael Baker International

Meeting Agenda: 10/23/2025 (10:00 AM - Noon CT)

1. Chairperson's Welcome (10:00 AM – 10:10 AM) [done]
 - a. AISC Antitrust Policy and Meeting Code of Conduct. [done]
 - b. Introductions (as needed). [done]
 - c. [Approval of Previous Meeting Minutes](#). No comments, approved.
2. Brief introduction of proposed G10.2 document (10:10 AM – 10:35 AM)
 - a. **Witte:** review of the intent of the document for new attendees. TG10 has had S10.1 for a long time and is written in spec language. G10.2 was conceived to provide more explanation and guidance for observation of girder erection in the field: what is noteworthy, problematic, regular behavior, etc. Audience is field staff performing inspection who should know basic bridge terms (not for the engineer).

Review of schedule that was set in 2024: final draft was due for end of 2025 – unfortunately not ready for ballot. Will need to update for realistic goals.
 - b. **Co-branding Document with AASHTO and NSBA:** Does this guide need to be co-branded with AASHTO?

- **Russo:** could set a precedent to undermine past efforts, cobranding adds weight of AASHTO, i.e. is “S” for cobranding, “G” for NSBA;
 - **Stith:** differentiate between recommendations (Cobrand) and general information (NSBA).
 - **Open discussion:** owner’s perspective – document is valueable whether cobranded or not – if the information is good, it will be used. NSBA was formed to create consensus documents, what cobranding shows is who has looked at it and reviewed it, and to the point of the committee existing.
 - **Garrell:** there are contractual agreements set in place if it is published by NSBA coming from this group. Based on how the document is intended to be used, in the field on a project, it makes more sense to have it go through the full review by AASHTO.
 - **Witte:** Will go forward with the full review process based on discussion and co-brand the document.
3. Summarize interim meetings of G10.2 development since Spring 2025 (10:35 AM – 10:40 AM)
- a. **Witte:** have had 6 interim meetings, efectively monthly, with great participation. Group created 300 pages of content including 212 pages of examples. Please let Brian know if you have not seen the document yet. Intention of small group was to establish the overall architecture.
Models and graphics: Authors requested to submit in native format for archiving by NSBA so that they can be updated or modified in the future as needed – they can be in whatever form you have them. Photo permission forms: need one for each photo; Witte to setup folders on Sharepoint site to house
Garrell: will review to see if there are concerns with current format of graphics, to help keep in front of it, and provide guidance.
Comment Resolution: have yet to close the comment loop with the authors. Witte accepted many changes that were clear or editorial, but many remain that need to be reseolved between the authors and the reviewers.

Small group review: some sections reviewed in more depth than others. This will be the focus for the remainder of the meeting (see bullet 5 below).

4. Review and discuss proposed schedule for G10.2 reviews and publication (10:40 AM – 10:45 AM)
5. Review comments from small group and TG10 members (10:45 AM – 11:45 AM)
 - a. **Document Size:** Is this too big?
 - **Jeck:** Not too big; it's apparent that people using the manual will pick out the sections they need.
 - **Russo:** it is all in here because it has value.
 - **Stith:** present counterpoint - there are some spots where it is written for the wrong audience and may need some clean up where something could be removed.
 - **Conclusion:** Review all sections and clean up for audience, but leave repeated sections since it will not be read as novel, but rather a reference manual.
 - b. **Repetition of sections:** seems to be repetition between sections (3, 5, and 6 in particular), look for ways to combine things.
 - **Russo:** maybe extended deadline is helpful: have a person who hasn't written too much of the content do the edit review of the document for tone, coherence, and consistency. The post-meeting version of the document is the one to be reviewed and will be distributed,
 - **Cisneros:** younger engineers outside of NSBA group would be good to review as the intended audience.
 - **Coletti:** will help Russo with review.
 - **Witte:** look at titles, content looking for a home, arrangement of sections.
Bearings: in 3, in 5.4, in 6.1 which looks rife for consolidation.
 - c. **Reinforce best practices for Section 4 examples:** some look good, but some need work.

- **Orton:** had added lots of things to consider as “should do” practices, should we cut those out?
 - **Witte:** Clarified that “Best Practices” refers to layout and formatting of the content in Section 4 and not best practices in the field.
 - **Stith:** but if this is intended to be used as a read what you need, then it might be best to repeat it different sections.
 - **Davidescu:** And if going that way, have more descriptive titles.
- d. 3.9.3 conflict with AASHTO:**
- **Orton:** wasn’t aware of the requirement, but shoring elevation should be dependent on your fit condition.
 - **Crampton:** this does appear to be different than what is being recommended in our document. Make sure reviewers pay attention to this.
- e. Section 5 content:** can we move this into 6? Or can 5 be turned into measurement templates in Appendix?
- f. 6.1.2.5 misplaced:** should this be moved? Does not read like it belongs there or it need much more information.
- **Davidescu:** move to shoring and just have it as an extension of that.
 - **Witte:** there is more jacking than just at shoring, could be in other directions and locations.
 - **Orton:** is jacking an observation? Is it just good to state that an inspector should expect to see jacks?
 - **Witte:** if you are erecting girders, then there are jacks on the project. But there is also certainly misuse of jacks. Need reminders that something that might look off is not necessarily a problem and jacking can be misused too.
- g. Definitions:** we need a section for this. Should follow AASHTO convention, but there are other colloquial terms used, like the “steel dances.”
- **Davidescu:** could put definitions to the side in a commentary column.
 - **Witte:** would be big formatting undertaking, additionally, this document is all commentary, not spec with commentary to the side.

- h. ***Doust comments based on review of entire document:***
 - **Doust:** 2 main issues – (1) remaining comments – need consensus between writer and reviewer. 2.1.4: section is missing, review recommends adding a section. Comments like this need time and may not be resolved immediately.
 - **Witte:** it is also possible that this will resolve itself with the complete document review.
 - **Doust:** (2) request for modification to figures.
 - **Witte:** make sure we are following Best Practices style guide.
 - **Russo:** all software output looks different, so it is what it is in most cases.
 - **Coletti:** Witte can scan comments and flag critical prior to Coletti and Russo reviews. Some onus back on the reviewers to reevaluate the comments based on the most recent version of the document.
 - i. ***General discussion: handwringing on the review process...***
6. Open discussion for other topics (11:45 AM – Noon)
- **Coletti:** for the record, the TG is not behind schedule. This is the process and based on experience the TG has done an amazing job!
 - **Witte:** many thanks to the authors and reviewers.
 - **General discussion:** Reminder of who the target audience is, all sections seem to be appropriate. Comment about taking out some isometric images – remember that these can be very helpful for the younger engineers who may not have the whole picture in their heads as well as the TG does. Please consider leaving them in the document – there is room for both. PennDOT volunteers to page through this after the Russo/Coletti review with their inspectors to provide another outside perspective.
Should plate sizes be included in Section 4: open for debate. Don't have to decide today.
7. Adjourn [12:55]



AASHTO/NSBA Steel Bridge Collaboration

TG 11 Design

Embassy Suites

Little Rock

Room Name: Rock Island 4-7

Task Group Mission: This Task Group aims to develop and maintain consensus guidelines to assist with the design of steel bridges and their components.

Task Group Leadership

Chair: Brandon Chavel - AISC

Vice Chair: Domenic Coletti - HDR

Meeting Agenda: 10/22/2025 (1:00 PM - 3:00 PM CT)

1. Chairperson's Welcome (1:00 PM – 1:10 PM) – start at 1:05 local
 - a. AISC Antitrust Policy and Meeting Code of Conduct. [done]
 - b. Introductions (as needed). [done]
 - c. Review of mission statement and current efforts
 - d. [Approval of Previous Meeting Minutes](#). [done – approved and seconded]
 - e. announcements:
 - i. IBC June 15-17 in National Harbor, MD. Abstracts are open until October 24th.
 - ii. NASCC: Georgia World conference center. Reminder that there are registration stipends for owners to attend. Highlighted the WSBS workshop including bolting demonstrations and virtual welding stations. GA will have a featured owner session
 - iii. Student Steel Bridge competition update for 2026. Always looking for volunteers. This is great workforce development opportunity.
 - iv. NSBA Prize bridge awards are due October 30, 2025.
 - v. Looking for bridge articles for MSC! Something that highlights use of steel for bridges are always welcome.
 - vi. Last meeting Ted Zoli discussed deck removal and girder buckling. Helwig has put together a research statement (still under review). Notes from N.

McCombs: concern is real world conditions during construction; look at stiffening strategies; there is a period between interim and final status that may not be captured by current analysis recommendations; conditions well below yield state; web stabilization with additional stiffeners; other

Saeed: how we can be sure that web buckling (web failure) caused the failure? The pictures seem to show flange failure. **B. Chavel:** we are not sure, that is the point of the submitted research plan. **K. Frank:** this is vertical flange buckling that comes from having a very slender web. This can't be prevented by vertical stiffeners. Web does not support the flange at this condition. **TH:** the deck is the compression zone. It is a complex stress transition and there may be a host of things that we could do to prevent it. **M. Culmo:** AASHTO committee is looking into this too. Many states don't even require analysis. We need to talk to the owners that this should be a concern for them. **R. Jeck:** confirms his analysis of these problems show that the web support at the flange is not there, it is effectively an unbraced flange. **F. Russo:** girder is now in partly composite configuration with heavy concentration construction loads in proximity. **D. White:** Coopers work in 67 and 68, Owen 70 – experiments showed buckling of the flange into the web. They all showed reaching the yield moment before the buckling of the flange. Running an eigenvalue on this in a model is a good start, but if one runs a full FEM it will show much more complex behavior post buckling. **Bob C.:** this is great! **Open discussion:** there are a variety of possible funding sources to leverage.

2. Presentation (1:10 PM - 1:45 PM)

a. TBD [n/a]

3. Guidelines for the Design of Cross Frames & Diaphragms (1:45 PM - 2:00 PM)

a. Balloting process and comment discussion

Chavel: update on ongoing effort. Thanks to members of TG11 who reviewed

and commented on the ballot! Comments were addressed by Chavel and Coletti. Main committee ballot was put through in July with additional comments. Gilmer went through with a big scrub that really helped improve the doc. AASHTO comments addressed by early Nov with responses before end of the year. In Jan 2026 will present responses to any major comments.

4. Phased Construction & Widening (2:00 PM - 2:45 PM)

Chavel: brief reminder of why the document was established. Last meeting reviewed the topics and organization of the proposed guide. This is volunteer effort, looking for volunteers to write the sections.

a. Review organization of topics

i. Review of volunteer assignments

Review of word document with the list of topics, see document.

General Comments: add integral bridge considerations to “other”? Have a specific section on long-narrow girder bridges? Add staged construction – cross-frame fit and differential deflection to skew and curved girder section. **F Russo:** this is derivative of some topics in other NSBA documents. Maybe we move a block of text from one of those documents to this one. **Chavel:** yes, but not to the extent needed. We can reference and not rewrite, but need everything in one spot. **Coletti:** is there a discussion on how to match existing geometry? **Chavel:** yes, under widening. **Cheng & Culmo:** add barrier design for temporary overhang (MASH compliance).

Assignments made in the word document

ii. Brainstorming on various topics and document needs

First draft by end of January. 1-2 months for first round of reviews. Chavel will collect the sections and send them out. Will work from a shareable drive. Will mimic cross frame process.

5. Open Discussion (2:45 PM - 3:00 PM)

a. Design issue discussions

M. Culmo: bolt holes in tension flanges – research is going well

D. White: NCHRP 12-128 – curved girder topics, led Don know if you have any comments.

Chavel: standard plans for steel bridges, open discussion for comments.

Fabricator members have been giving them to contractors for pricing. **Culmo:** very useful, looking forward to SIMON release. **A. Ream:** steel bridge design handbook being updated by HDR; under review and hope to be out by the end of 2025. Merged filed splice design as well as tub girder design and stability design. Examples are all updated as well. **Chavel:** two other documents in the works: grade crossing guideline document – in final review – and working with Valmont on press break tub girder design guide. **Culmo request:** change transition locations from dimension from left to a % of span. **Russo:** new input form for cross frame spacing. Grubb working with the software company to check the SIMON code and eventually they will give it to Frank to rerun the standards to check for how the updates affect them.

Jerry S.: looking for guidance for sign structures attached to the facial of the girder.

D White: given standard plans, do the girder designs really need to change that much for skew? Asking about up to 60-degrees. **Chavel:** no, but cross frames will change. In NSBA presentations, discuss good to start with the standard plans still and then use those for refining analysis. **Saeed:** what is the target D/C ratio? **Russo:** the answer is 1.0, but they vary based on the needs of the design. If an owner needs something different, use your PE and adjust the design. These are only a starting point.

K Frank: considering tabulated bolts table and angle eccentrically loaded in compression. Would it be useful to have in the bridge industry? **General discussion:** currently use the AISC as a starting point, so would be good to have AASHTO version. What is the format that would be convenient? Spreadsheet

for pulling into other design tools or PODF table would both be good. TG11 supports the initiative.

6. Adjourn [2:45pm Central]



AASHTO/NSBA Steel Bridge Collaboration

TG 12 Design for Constructability and Fabrication

Embassy Suites
Little Rock
Room Name: Rock Island 4-7

Task Group Mission: This Task Group primarily focuses on addressing the questions that have been and are continually asked concerning the constructability of steel bridges according to the latest practice for steel mills, fabrication, detailing, erection, and design.

Task Group Leadership

Chair: Russell Jeck - GZA GeoEnvironmental Inc.

Vice Chair: - TBD

Meeting Agenda: 10/22/2025 (9:00 AM - Noon CT)

1. Chairperson's Welcome (9:00 AM – 9:15 AM)
 - a. AISC Antitrust Policy and Meeting Code of Conduct. **Done.**
 - b. Introductions (as needed). **Done. Approximately 50 attendees total.**
 - c. [Approval of Previous Meeting Minutes](#). **Done.**
2. Chesapeake Bay Bridge - Accelerated Construction Presentation by George Patton of H & H (9:15 AM - 10:15 AM) **Done. Very interesting presentation. New exodermic deck. Complex constructability. Many questions afterwards.**
3. Brooklyn Bridge - Damage from Ship Collision by Russ Jeck (10:15 AM - 10:45 AM) **Done. Most of damage from the mast of the tall sailing ship collision was to the steel traveler system suspended under the bridge deck. There was minor damage to the bridge deck system. All damage will be repaired. Russ noted that trucks are not allowed to drive over the bridge due to posted 3 ton weight limit. Russ also noted that the structural floor system of the existing bridge is composed of relatively "light" built-up members.**
4. Break (10:45 AM – 10:55 AM)
5. Future Items for Consideration in Next Document (10:55 AM - 11:30 AM)
 - a. AASHTO Cross-frame bracing requirements for strength and stiffness during deck replacement

- If half-width deck is removed for replacement, and the remaining half of the deck continues to carry live load, the center cross-frame experiences significant differential deflection. Half of the bridge is composite and the other half is non-composite. Significant cross-frame forces occur in order to stabilize the non-composite girders against buckling and accommodate the differential buckling.
- Todd Helwig commented that the appropriate load factor to use for dead load is 1.25, not 1.40 (as Russ was requested to use by an Owner).
- Frank Russo commented that stability of the non-composite girders is not an issue as they are connected to a rigid half-deck, and that the concern should focus solely on the differential deflection.
- It was noted that the non-composite girder closest to the deck removal line can experience significant live load transfer from the traffic running on the adjacent half-deck.
- Karl Frank commented that excessive cross-frame forces during partial deck removal/replacement can be mitigated by strategically removing cross-frame diagonal members in the bay near the concrete removal line.
- Brandon Chavel noted that TG11 is addressing this in their cross-frame design guide, which will include phased construction including partial concrete deck removal/replacement (including appropriate load factors to use).
- Don White commented that the upwards rebound of the girders when the deck is removed could be considered a locked-in force, and if so, has a load factor of 1.0.

On a separate topic - Deck overhang brackets used to support concrete deck forms impart lateral load and rotation on the exterior girders. Kansas DOT uses a 1% rotation limitation on the exterior girder which is considered reasonable/appropriate. Russ suggested that this 1% limitation be stated in the design guide being developed for overhang brackets.

Russ stated that recent AASHTO 10th Edition updates may necessitate an update to our G12 document that was published a couple years ago. Frank Russo and Brandon Chavel said this is likely prudent. A discussion of this is being included in the cross-frame design guide being developed , so referring to it is likely a good option.

- Domenic Colleti mentioned that bolted field splice design/detailing recommendations should be included in the G12.1 document. Currently it is not. It was previously discussed for inclusion with Christina.

6. Open discussion - Designing for Future Needs (11:30 AM - Noon)

7. Adjourn Ended meeting at 11:40 am.



AASHTO/NSBA Steel Bridge Collaboration

TG 13 Analysis of Steel Bridges

Embassy Suites

Little Rock

Room Name: Rock Island 4-7

Task Group Mission: This Task Group focus has been the development of guidance on the issues related to steel girder bridge analysis and to educate Engineers so that they can better make decisions for their own projects.

Task Group Leadership

Chair: Deanna Nevling - HDR

Vice Chair: Francesco Russo - Russo Structural Services

Meeting Agenda: 10/23/2025 (8:00 AM - 10:00 AM CT)

1. Chairperson's Welcome (8:00 AM – 8:10 AM)
 - a. AISC Antitrust Policy and Meeting Code of Conduct.
 - b. Introductions (as needed).
 - c. [Approval of Previous Meeting Minutes](#).
 - i. Meeting minutes were approved by the TG.
2. General Announcements (8:10 AM – 8:25 AM)
 - a. Conferences/Research/Publications
 - b. NSBA Update – Brandon Chavel
 - i. Brandon provided updates on various new NSBA publications and upcoming work by NSBA. Brandon also noted the Bridge Education efforts related to Steel Bridge Forums as well as the support of the Purdue Bridge Engineering Program.
 - c. FHWA Update – TBD
 - d. TRB AKB20 (Steel Bridges Committee) Update – Brandon Chavel
 - i. Brandon noted that the TRB has undergone some changes and the committee structure has changed. The next meeting is in January 2026.
 - e. AASHTO Bridge Update (T-14 Structural Steel Design) – Tony Ream

- i. Tony updated the TG on the various ballot items that have gone through the AASHTO COBS Steels and Metals committee.
 - ii. Todd Helwig also talked about changes and improvements that will be upcoming for stability bracing and lean on bracing guidance.
- 3. “Fern Hollow Collapse Analysis,” Frank Armont (8:25 AM – 8:55 AM)
 - a. Frank spoke about the analyses of the Fern Hollow bridge, explaining how the bridge collapsed. This included discussions on the field investigation, global static analysis, global collapse analysis, local analysis of the SW Column Leg, and the conclusions from the analysis. Analysis included models with section loss for the column leg. Section loss was based on 3D scan data of the members. Material stress-strain behavior based on FHWA test data for yield, ultimate, and fracture.
 - b. General conclusions included:
 - i. Severe corrosion at base of frame leg was the most significant contributor to the collapse.
 - ii. Global analysis used to determine demands at time of failure
 - iii. Global collapse analysis was used to confirm post-collapse bridge behavior assuming leg failure matched field observations.
 - iv. Failure modes in the local and global analysis models were consistent with field observations.
 - c. Local analysis conclusions included:
 - i. Failure of the tie at the base of the leg would precipitate the collapse of the bridge
 - ii. Alternate load path exists thru flange bending, but sudden failure of the tie plate would result in dynamic effects exceeding capacity
 - iii. Results are sensitive to section loss and elongation capacity of the tie plate.
- 4. “Eigenvalue Buckling Analysis - Guidance in the New AASHTO Nonprismatic Steel Girder Design Guide,” Don White (8:55AM to 9:25 AM)

- a. Don's presentation reviewed this new design guide. The design contains 8 examples that address various different design attributes that can be encountered during design.
 - b. Don noted that the guide is only for LTB design verifications, not all design checks; and serves as a companion to the AASHTO LRFD BDS 10th edition. The guide uses moment diagrams and envelopes from bridge analysis at 1/10 span locations. There are full calculations for each example provided only when Method C (FEA linear bifurcation analysis) is used to obtain the elastic buckling load multiplier. Methods A and B illustrations focused solely on the corresponding elastic buckling load multiplier estimates, then showing just the results of the remaining full calculations.
 - c. Don also reviewed some of the examples that are part of the guide.
5. G13.2 Guidelines for Steel Truss Bridge Analysis (9:25 AM – 9:30 AM)
- a. Published!
 - i. Deanna noted that this new guideline was published earlier this year.
6. Software Validation and Checking Complex Models (9:30 AM – 9:45 AM)
- a. Survey results white paper and MSC article
 - i. Deanna briefly highlighted this effort. She will be sending out meeting invites soon to keep working on this effort.
 - b. Checklist – review volunteers
 - i. Deanna briefly noted that she will be asking for volunteers for this effort.
7. TG13 New Initiatives (9:45 AM to 10:00 AM)
- a. Deanna briefly noted these items below
 - b. TG13.1 Updates
 - c. Buckling and Global Stability Analyses
 - d. Analysis of Arches
8. Adjourn
- a. Meeting adjourned at 9:58 AM



AASHTO/NSBA Steel Bridge Collaboration

TG 14 Field Repairs and Retrofits

Embassy Suites

Little Rock

Room Name: Rock Island 4-7

Task Group Mission: This Task Group primarily focuses on providing practical solutions for design and implementation of field repairs and retrofits of existing steel bridges.

Task Group Leadership

Chair: Kyle Smith - GPI

Vice Chair: Nick Haltvick - Minnesota Department of Transportation

Meeting Agenda: 10/22/2025 (3:00 PM - 5:00 PM CT)

1. Chairperson's Welcome (3:00 PM – 3:10 PM)
 - a. AISC Antitrust Policy and Meeting Code of Conduct.
 - b. Introductions (as needed).
 - c. [Approval of Previous Meeting Minutes](#).
 - i. There were no comments on the Spring Meeting minutes, thus approved.
2. TG-14 and G14.3 Overview (3:10 PM - 3:20 PM)
 - a. Reviewed the mission statement and G14.1 and G14.2 guideline documents.
 - b. G14.3 – discussed the approval process in place. It will not be a traditional Collaboration guideline, but a document that will be on the NSBA website.
3. Discuss G14.3 Detail Sheets (3:20 PM - 5:00 PM)
 - a. Providing sample details “as-is” for users to review. Provide commentary on the details.
 - b. Status – 1 User Guide is ready for ballot, 6 details ready for ballot. 8 detail sheets have been reviewed, and are awaiting revision. 5 detail sheets will be reviewed today. 30 details received from DOT survey that need detail sheets to be developed.
 - c. Will published when we have about 25 details ready.
 - d. User Guide – no additional comments at the meeting
 - e. Partial Length Girder Replacement Detail

- i. Detailing – this is a custom detail
- ii. Installation – Use a check on General contractor only
- iii. Adjustability – leave as is
- iv. Commentary
 - 1. Reviewed the comments and walked thru them one by one. In the Bluebeam file, Kyle noted the ones that the TG was in agreement with, and those that were deemed to not be persuasive.
 - 2. Brian W. – General comment – the commentary is too much. We should reduce it. Try to keep just to the detail as a starting point for engineers.
 - 3. Mike D. – some of the commentary may be repetitive from detail to detail. Perhaps, it is worthwhile to have some general commentary that applies to all details.
- f. Overall Categories – the work Adjustability. Should this be Adaptability? The section needs clarified nonetheless.
 - i. Should we use the term field adjustability?
- g. Heat Straightening Detail
 - i. Reviewed the comments and walked thru them one by one. In the Bluebeam file, Kyle resolved the comments based on input from the TG and made additional notes as needed.
 - ii. Commentary should reference the FHWA manual and note jacking simultanesouly while applying the heat is not recommended.
 - iii. Note that we may want to add – these are conceptual details that are porvided by an owner, and are to be used as a concept. Designer should evaluate the feasibility of the conceptual detail for their particular project.
 - iv. Remove the detail for the crack arrest hole, and remove from the keywords section.

v. Consider adding a comment to inspect for cracks in the flange.

4. Adjourn

a. Meeting ended at 4:48. Kyle noted some additional virtual meetings will be needed to resolve the comments.



AASHTO/NSBA Steel Bridge Collaboration

TG 15 Data Modeling for Interoperability

Embassy Suites

Little Rock

Room Name: Rock Island 3

Task Group Mission: This Task Group's primary focus is on facilitating the development of bridge industry consensus standards for data description, modeling, and interoperability for integrated design, construction, and lifecycle management of bridges (i.e. BIM).

Task Group Leadership

Chair: Aaron Costin - University of Florida

Vice Chair: Grant Schmitz - HDR

Meeting Agenda: 10/23/2025 (10:00 AM - 1:00 PM CT)

1. Chairperson's Welcome (10:00 AM – 10:10 AM)
 - a. [AISC Antitrust Policy and Meeting Code of Conduct.](#)
 - b. Introductions (as needed).
 - c. [Approval of Previous Meeting Minutes.](#)
 - i. Approved
2. Announcements (10:10 AM – 10:20 AM)
 - a. Overview of TG
3. Related Efforts Update (10:20 AM – 10:50 AM)
 - a. Pilot projects
 - i. FHWA Grants
 1. Iowa DOT
 2. PennDOT
 - b. TPF BIM for Bridges Phase 2
 - c. NSBA Involvement
 - i. [Current Working Group: Jessican Wang Caman, Russel Boss, Ben Arcinega Utah Pacific Randy Harrison W&W AFCO, Tom Beam High Steel Structures, Mike Worsh Stupp,](#)
4. TG15 IDM (10:50 AM – 11:20 AM)

5. Data Dictionary Template Overview (11:20 AM – 11:50 AM)
 - a. BuildingSMART Data Dictionary
 - i. Bsdd
 - ii. USDD
 1. Enhances current IFC Model
6. Working Group (11:50 AM – Noon)
7. Adjourn



AASHTO/NSBA Steel Bridge Collaboration

TG 16 Orthotropic Deck Panels

Embassy Suites

Little Rock

Room Name: Rock Island 3

Task Group Mission: This Task Group aims to establish an Orthotropic Steel Deck (OSD) panel design that can be cost effectively produced in the United States for the bridge market.

Task Group Leadership

Chair: Sougata Roy - SOCOTEC Engineering, Inc.

Vice Chair: Frank Artmont - Modjeski & Masters, Inc.

Meeting Agenda: 10/21/2025 (9:00 AM - Noon CT)

1. Chairperson's Welcome (9:00 AM – 9:10 AM)
 - a. [AISC Antitrust Policy and Meeting Code of Conduct](#). **Done.**
 - b. Introductions (as needed). **Done. 11 people total.**
 - c. [Approval of Previous Meeting Minutes](#). **Approved.**
2. 3.General updates and announcements (9:10 AM – 9:20 AM)
 - **Currently there appear to be no recent bridge OSDs fabricated in USA.**
 - **Regarding moveable bridges, steel grid deck is difficult to obtain, so the time could be good for using OSD.**
 - **Likely need some sort of OSD standard details in order for domestic fabricators to get interested.**
 - **Current steel tariffs could make it more attractive for domestic fabricators to do OSDs.**
 - **ISC (Gary IN), Stinger (AZ) and expansion joint fabricators seem to be good potential fabricators for OSD.**
 - a. **Workshop at IBC, 2025 This went good overall. Next step is to potentially present or have a workshop at TRB. TRB is planned to take place on 1/11 – 1/15/26. OSD presentation should be considered for WSBS 2027 conference (Sougata). Also, should be considered to present at North Central States Bridge Consortium (Terry Logan), NSBA Steel Bridge Forums (Duncan Paterson), Moveable Bridge Conference (Keith Griesing), International Cable Supported Bridge Operators Conference (Frank Artmont).**
3. Review of mission statement: (9:20 AM – 9:30 AM) **No comments, so stays the same.**
4. Short Span Orthotropic Update (SSSBA) collaboration update (9:30 AM – 9:35 AM)
 - **No update since Dan Snyder is not present. Justin Dahlberg also not present.**

5. General update on ongoing projects/research (9:35 AM – 9:45 AM)
 - Frank Armont gave a presentation on the development of short (140' and under) span OSD bridge design standard details as part of the recent FHWA research project on Level 1 OSD design. Includes open rib deck, floorbeams, girders, barriers, and construction sequence. Can be hot-dip galvanized if desired. Wearing surface weight included in design. See attached slides.
6. Break (9:45 AM – 10:00 AM)
7. Presentation: (10:00 AM -10:45 AM)
 - a. PPC Wearing Surface for Orthotropic Decks – Casey Rafter, VP, Sales, Sika
 - PPC = polyester polymer concrete.
 - Casey is proposing that PPC is an ideal material to be used for the OSD wearing surface. Showed history of use and performance.
 - He made comparisons to ROSPHALT and Epoxied Modified Asphalt Concrete.
 - PPC is cost competitive and claims to perform superior compared to other options.
 - See attached slides.
8. Review of Committee Revised Goals – Next steps. (10:45 AM -11:15 AM)
 - a. Targeted presentations (20 minutes each) due date 02/01/24
 - i. Owners – Sougata Roy (lead), Terry Logan
 - ii. Designers – Frank Artmont (lead), Justin Dahlberg, Keith Greising, Sougata Roy
 - iii. Fabricators – Terry Logan (lead), Chris Haberle, Ronnie Medlock
 - Done, as follows. Sougata quickly ran through the Powerpoint presentation (4 hours total) that was given at the IBC conference earlier this year. It covered all aspects of OSD bridge decks including history, fabrication, performance, past issues, welding, cost, etc. It was well received.
 - b. MSC Article – Justing Dahlberg (lead), Frank Artmont, Duncan Patterson, Terry, Logan, Ronnie Medlock, Sougata Roy, Tom Murphy – published **Article is done and published. It was well received.**
 - c. Filling the Knowledge Gaps **No discussion.**
 - d. Rough plans for FHWA optional task, Justing Dahlberg – update: **This has been done, as M&M has completed the optional tasks.**
9. Discussion on State of Practice Synthesis Document (11:15 AM – 11:50 AM)
 - a. Review sections

- Sougata reviewed the document outline and schedule for completing this document/guide. He emphasized that this outline has been “hanging around” for years and now needs to be completed.
- Sougata asked Terry Logan about completing the fabrication portion of this document, Terry said he has lost interest in working on this. He also stated that most fabricators are not interested in a long document such as this proposed one.
- Keith suggested we consider changing the focus of the document. Sougata’s opinion was that this change of focus is not acceptable, however, a change in volume is acceptable.
- Frank Armont suggested that the document needs to be completed and obtain an AASHTO approval. He suggested that the document is essentially a written version of the Powerpoint presentation recently given at IBC.

b. Monthly webinar meetings schedule

10. Old business and additional discussion (11:50 AM – Noon)

11. Adjourn Meeting adjourned at 12:10 pm.



AASHTO/NSBA Steel Bridge Collaboration

TG 18 Duplex Stainless Steel

Virtual

9/30/25, 10:30am – 12:30pm EST

1. Committee Business (10:30am - 10:50am)

a. AISC Antitrust Policy and Meeting Code of Conduct

b. Introductions of Attendees

- Catherine Houska
- Jason Provines
- Nancy Baddoo
- Juan Sobrino
- Andy Personett
- Bret Clark
- Gary Coates
- Karl Frank
- Randy Harrison
- Francisco Meza
- Peter Ault
- Ted Bush
- Heather Gilmer

c. Approval of [Previous Meeting Minutes](#)

- Gary had a question about welding interpass temperature. Jason said they would discuss this during the meeting.
- Minutes were then approved.

d. Review of TG18 Specification Progress and Future Schedule

- Creation of six guide specifications for duplex stainless steel. All 6 will be a complete package for bridge owners to use if they desire to use duplex stainless steel.
- The Duplex Materials (S18.1) and Duplex Design (S18.2) Specs (2 of the 6) are essentially completed and in the process of review/incorporation by AASHTO.
- The Duplex Bolting and Welding Specification are next in line for completion.
- Tony suggested that NSBA can promote Duplex Stainless Steel at Steel Bridge Forums. NSBA plans to hold 10+ Steel Bridge Forums in 2026 scattered throughout the country. Jason/Nancy to send Tony two (2) Powerpoint slides for him to use at the Michigan Steel Bridge Forum on 10/8/25.

e. S18.1 and S18.2 Cover Design Art

- Nancy showed the proposed cover to the specification document with a variety of duplex stainless steel photos during fabrication and installation. The same photos will be used for all of TG18 specifications to indicate that they are a family of specifications. Subtle differences will be made on each cover page to indicate that they are a different specification.

2. Discuss Duplex Welding Spec (10:50am - 11:30am)

- The group agreed to move all handling and lifting procedures for duplex stainless steel from the Welding Spec to the Fabrication Spec to centralize cleaning and contamination control, which is critical given duplex steel's sensitivity to carbon contamination.
- A clarification was made about wire brushes used for slag removal, specifying wire materials must have corrosion resistance equivalent to the base metal, preferably 316 stainless steel, 2205 duplex stainless steel, or nickel alloy 625, to avoid embedded contaminants causing corrosion or weld defects.
- The group resolved to refer to D1.5 Bridge Welding Spec for weld undercuts, as these already establish appropriate tolerances and there is no strong evidence that undercuts cause crevice corrosion in bridge applications.
- For mislocated holes, either weld repair or use of pre-tensioned bolts meeting duplex bolting specs is allowed, with emphasis on pretensioning to prevent moisture entrapment and improve fatigue resistance. A suggestion was made that the reference regarding the pretensioning of the bolt should be to the Design Spec.
- The post-weld heat treatment limit was increased from 150°F to 200°F to better align with real-world conditions and avoid conflicts with environmental exposure, as highlighted by Gary and Karl.
- Temporary marking materials like crayons are permitted during fabrication but must be fully removed prior to on-site welding and project completion, following AISC 370 guidance to avoid corrosion and aesthetic issues.
- The group decided to retain plug and slot welding clauses with the caveat that such welds are only allowed if specified or approved by the engineer, reflecting current bridge code restrictions and concerns about fatigue and inspection challenges. These are also not issues specific to duplex stainless steel, so they need not be addressed in the duplex Welding Spec.

3. Discuss Duplex Bolting Spec (11:30am - 12:20pm)

- The new bolting specification was developed as a standalone document modeled on ASTM F3125 to cover gaps in ASTM A1082 related to washers, lubrication, proof load testing, and tensile strength, aiming for clarity and usability by bridge engineers.
- The specification will focus solely on imperial units, as supported by Karl and others, because most US and Canadian bridge bolts use inches, and metric introduces complications in thread pitch and tensioning.
- A firm consensus was reached to require bolting assemblies to be supplied pre-lubricated, as lubrication is critical to prevent galling and ensure proper tensioning, with suppliers expected to provide lubrication and ROCAP test results confirming performance.
- The TG18 specifications will initially only cover turn-of-nut installation, deferring combined method installation for future editions to avoid delaying publication, acknowledging combined method bolts and testing protocols are not widely available or standardized in the US.

- Feedback from supply chain contacts will be sought to confirm feasibility of requiring pre-lubricated assemblies, with no current objections expected based on supplier experience.
- The scope of the bolting spec will primarily address pretensioned bolted connections, as almost all structural bridge bolts require full pretension.
- Discussions highlighted the need for clear guidance on installation torque and testing, referencing ASTM F3125 protocols where applicable, to ensure field and shop tensioning meet design pretension values.
- The draft currently references ASTM F436 (carbon steel) for washer hardening, which was identified as inappropriate; the group suggested considering the guidance from AISC 370 specifying acceptable low-temperature carburization or equivalent treatments to avoid damage to duplex stainless steel washers.
- There is recognition that duplex stainless steel washers meeting ASTM A240 grade UNS S32205 are commonly used, manufactured by stamping or cutting from sheet stock, and must have hardness higher than bolts while maintaining corrosion compatibility.
- Ted Busch offered to share the exact washer, bolt, and nut material specifications used in past projects meeting Buy America requirements,
- The bolting spec will explicitly require compatibility of all components in terms of corrosion resistance and mechanical properties, ensuring assembly integrity and longevity under bridge service conditions.

4. Discuss Duplex Fabrication Spec (12:20pm - 12:30pm)

- The Fabrication Spec is underway, closely based on AASHTO LRFD Steel Bridge Fabrication Specifications including 2024 and 2025 interim revisions, with supplementary duplex-specific modifications aligning with AISC 370 and IMOA guidelines.
- The team aims to complete the draft within the next couple of months to accelerate the overall specification package delivery, anticipating the Construction Spec to be shorter and follow later.
- Integration of the requirements in the Fabrication Spec with the requirements in the Welding Spec is critical, especially regarding maximum heating limits during processes like girder straightening, where temperatures may exceed the 200°F limit agreed for welding, presenting a potential conflict that requires resolution.
- Expertise from TG18 members will be heavily relied upon to refine fabrication provisions, ensuring compatibility with duplex stainless steel's material sensitivities and welding constraints.

5. Meeting Adjourned (12:30pm)



AASHTO/NSBA Steel Bridge Collaboration

TG 19 Movable Bridge

Embassy Suites

Little Rock

Room Name: Rock Island 4-7

Task Group Mission: This task group develops and maintains guidelines for the design and construction of movable steel bridges. The focus is on structurally efficient designs that minimize span weight and integrate effectively with machinery, lightweight decks, and other movable components. The guidelines also address constructability and achieving required machinery fits and tolerances during fabrication and erection. Mechanical and electrical systems are not covered.

Task Group Leadership

Chair: George Patton - Hardesty & Hanover, LLC

Vice Chair: Frank Artmont - Modjeski & Masters, Inc.

Meeting Agenda: 10/23/2025 (12:00 PM - 1:00 PM CT)

1. Chairperson's Welcome (Noon – 12:10 PM)
 - a. AISC Antitrust Policy and Meeting Code of Conduct. [done]
 - b. Introductions (as needed). [done]
 - c. [Approval of Previous Meeting Minutes](#). [n/a]

Paton: Jim Philips will provide a summary of NCHRP 10-137.

J Phillips: purpose of NCHRP 10-137 is to develop construction requirements for moveable bridges. The overarching goal is to implement the resulting document as an AASHTO Construction Specification. Project is now completed through interim report number 1 (Task 4 of 11). Initial Tasks, Literature review Key finding: *information needed is not in published documents, information will need to come from sample projects*. Project has no intent to recreate what is already in existing references. Summary for Task 3: proposed research plan has been proposed, and NSBA task group is noted as a stakeholder. Delivery outline is presented and is consistent with AASHTO format.

Reach out to Jim if you are interested in seeing the details of the outline deliverable being proposed. The study will be focusing on 3 major bridge types:

bascule, swing, and vertical lift, and the most common configurations thereof.

The owner questionnaire is still available to anyone who would like to fill one out to help with the project. The acknowledgement and disclaimer for the NCHRP project was presented in full.

Q&A: Patton: great introduction and opportunity for collaboration with this TG is great. *Carlson:* what is the difference between TG work and NCHRP project, can we establish that yet? *Patton:* that will be the topic for the remainder of our time at this meeting.

2. New committee open discussion (12:10 PM – 12:45 PM)

a. Goals, objectives and future direction

Patton presentation: develop standard practices, best practices; also have a goal for education and understanding, leading to an NSBA guide document.

Present a list of talking points:

Moveable bridge design: acknowledge that many of us are using outdated information and practices (examples presented). Disadvantages include complex fabrication and higher steel cost (others also mentioned). Transition to modern practices in other parts of the world (examples presented). Advantages include simplified fab and erection, lower steel unit costs (other example presented).

Visual example of bridges from 2002 (modern) and 2014 (detail intensive) and some European examples with more elegant detailing. Other types of cleaner detailing for trusses (e.g. perforated girders, gussetless).

NSTMs: common on moveable bridges; can we eliminate them? Some strategies are presented. Appear to be opportunities to advantage of load path redundancy.

Other Important considerations: Machine alignment; machine fit and finish; structural steel vs. machinery alignment; structural deformation effects on machinery; machining of steel framing; machinery component positioning.

Types of bridges: various needs for each type that Phillips discussed

Turned Bolts: custom bolting; reduction of bolt tensioning forces; other

considerations (e.g. fitup tolerances for large grips; coatings on faying surfaces; spot facing); strategies to minimize turned bolts. Discuss different types and locations where use of turned bolts could be evaluated.

Survey techniques; purpose and details of survey controls; what are critical dimensions; alignment of DOF; factors that affect alignment; measurements and documentations; shop procedures; shop machining considerations; typical machine setups and measurements; best practices for machining; machinery fits and shrink fit options; measurements and documentations for surveys; best practices to reestablish shop alignment in the field; relationship between components; effect of structural deformation on machinery; equalization of live load shoe reactions; erection procedures.

Q&A: **Griesling**: curbs – can't always match MASH, i.e. what are the exceptions/exclusions from AASHTO that are necessary. **Alison**: presentation covered what the fabricators wanted to discuss; one we didn't mention is wire ropes. **Patton**: NSBA suggested that the goal is to work on the interface between machiner and the structure and not get too outside the scope of steel bridges. **Harrel**: shivs are a large and important part of moveable design and construction and should be included. **Patton**: don't want to ignore machinery, just don't want it to be the focus. Another topic: what is importance of fit up of rack when there will be field deformations? **Jeck**: racks on a highway bridge are still a heavy lift system with many options for assembly. **Allison**: in light of the NCHRP and existing AASHTO document – should we concentrate on certain topics? **Patton**: can envision multiple outcomes: be consistent with other works; for action items, need team to help with guiding TRB through review, opportunity for much more commentary for this TG to present good/best practices.

Next steps: smaller group interim meetings. Presentation can become the outline for an NSBA document; can use that for assignments. Goal for spring is to have that outline for the next meeting. Looking for volunteers to help with small group meetings to push thing forward. **Artmont**: obvious support for

NCHRP, but can focus on the design side “here is what you need to know for designing a moveable bridge” then after NCHRP publication, start to fill in the knowledge gaps. **Warncke:** Can we start with an analysis document; how to design moeble? **Harrell:** existing documents leave a lot of room for interpretation – think about a pocket companion giude to the AASHTO document. **Open discussion:** Or even discuss how do ratings work? Don’t get too fancye with load ratings. Teach folks not to get too creative with interpretaion of structural systems. Is there room for seismic considerations? **Chavel:** BP for fabricators is likely the best target. Layout everything you want and then pick the top 15 items as a goal for the TG (looks like 20yrs of work that was just laid out!). Use the focus group to identify those priority topics. Patton: pleasee reach out with interest to work on the TG or the focus group.

- b. Ongoing related work by TRB/AASHTO
 - c. Topics for movable bridge design guidelines
 - d. Topics for movable bridge construction guidelines
3. Action items and assignments (12:45 PM – 1:00 PM)
 4. Adjourn [1:01pm]



AASHTO/NSBA Steel Bridge Collaboration

MC Main Committee

Embassy Suites

Little Rock

Room Name: Rock Island 4-7

Task Group Mission: The Collaboration Main Committee provides oversight and guidance for all Task Groups. A meeting of the Main Committee will take place at the end of each Collaboration meeting.

Task Group Leadership

Chair: Ronnie Medlock - High Steel Structures

Vice Chair: Natalie McCombs - HNTB

Meeting Agenda: 10/21/2025 (1:00 PM - 3:00 PM CT)

1. Chairperson's Welcome (1:00 PM – 1:10 PM)
 - a. AISC Antitrust Policy and Meeting Code of Conduct.
 - b. Introductions (as needed).

Ronnie reviewed the origins and purpose of the Collaboration for the new attendees. This is the first time the Main Committee met on the first day of the week.

- c. [Approval of Previous Meeting Minutes.](#)

Minutes were approved.

2. Task Group Reports - Approximately five minutes each (1:10 PM – 2:20 PM)
 - a. TG 1 – Randy Harrison (W&W | AFCO Steel)
 - The group is currently working on two guidelines, including updates to G1.1, Approval of Shop Drawings. Discussion focused on whether certain detailing steps add value to the approval process. Randy distributed comments on the draft document to the group for review and discussion this week.
 - New design drawings (approximately six sheets) are being redrawn in AutoCAD, with comments collected and incorporated into the revisions. Geoff Swett reminded the group of issues related to presenting details on

separate sheets, noting that individual details or drawings may need to be sealed or stamped. The topic was tabled for further discussion during the TG1 meeting.

- b. TG 2 – Heather Gilmer (Pennoni)
 - The group is working on two documents: the AASHTO Fabrication Specification and G2.2. A draft of the Fabrication Specification was submitted to AASHTO for review, and the task group has addressed several comments received. Discussion centered on check assemblies and owner concerns about potentially losing oversight, as well as match marking practices. This topic was tabled pending further discussion with machine manufacturers.
 - For G2.2, discussions included topics such as improper preheat and member misalignment. The group also plans to reproduce certain drawings in the document for improved clarity.
- c. TG 4 – Jamie Hilton (KTA-Tator, Inc.)
 - G4.1, QC/QA Guidelines, is in the final stages of typesetting and awaiting a cover.
 - The group is also developing S4.3, a specification for Owner’s Inspectors (third-party firms), intended to help owners incorporate inspection requirements into their own specifications. This document was previously balloted but pulled for further revision. The task group continues to work through comments received.
- d. TG 8 – Johnnie Miller (KTA-Tator, Inc.)
 - Johnnie Miller was unable to attend, so Derrick Castle provided the update.
 - The task group has been renamed Corrosion Protection.
 - S8.1 has advanced to the AASHTO Steel and Metals Committee for review. The next focus will be S8.2, Thermal Spray Coatings.
 - The group is also developing guidance on detailing for coatings and understanding how coating systems influence design decisions.

- Additionally, the NSBA Uncoated Weathering Steel Guide has been provided to the AASHTO Steel and Metals Committee for preliminary review, with a target publication date of 2027 (COBS cycle).
- e. TG 9 – Michael Culmo (CHA Consulting, Inc.)
- G9.1 was last published in 2022. The group is developing a new chapter on inspection and maintenance, including sections on repair and replacement. Work has also begun on a new document covering large-movement expansion joints.
 - While small-movement joints are not unique to steel bridges, the group believes guidance is needed on girder detailing, tolerance adjustability, and maintenance access.
 - These topics are particularly relevant for long, continuous-span bridges. Volunteers will be solicited to draft specific sections.
 - A proposal to rename the task group to include the word “Components” was discussed but not approved.
- f. TG 10 – Brian Witte (Parsons)
- TG10 has been holding interim calls to develop G10.1, a collection of 24 case studies covering various plate girder bridge configurations.
 - Approximately 20–30 members are actively contributing, and a Task Group ballot is expected by late 2025 or early 2026.
 - The intent is for this to be published solely as an NSBA document, not through AASHTO COBS.
- g. TG 11 – Brandon Chavel (NSBA)
- G11.1 has been submitted to the AASHTO Steel and Metals Committee for comment. Once comments are reviewed and incorporated, an updated version will be posted in December.
 - The group is also developing a new phased construction guideline and will use the upcoming meeting to identify writers for individual sections.
- h. TG 12 – Russell Jeck (GZA GeoEnvironmental, Inc.)

- The committee recently published its Straddle Bent document and is now refocusing on G12.1, ensuring consistency with updates introduced in the AASHTO LRFD 10th Edition.
 - This week’s meeting will include several presentations and discussions on staged construction challenges and overhang design guidance.
 - Coordination between TG11 and TG12 may be beneficial given overlapping topics.
- i. TG 13 – Deanna Nevling (HDR)
- G13.1 was last published in 2019, and G13.2 (Truss Design) was published earlier this year.
 - Current work focuses on a software survey, a white paper, and a Modern Steel Construction article summarizing results.
 - The group is also developing a checklist for evaluating structural analysis software and will host two technical presentations during the meeting.
 - Future work may include a document on arch bridges.
 - Deanna also referenced a recent NCHRP Synthesis Report on Quality Processes for Bridge Analysis Models, which surveyed state DOTs on model review practices.
- [NCHRP Synthesis 602 – Quality Processes for Bridge Analysis Models](#)
- j. TG 14 – Kyle Smith (GPI Construction Engineering)
- The group currently has two published documents. G14.2 covers height adjustments and jacking.
 - Work is ongoing on G14.3, a database of repair details. Six detail sheets have been completed, with eight more nearing finalization; five will be reviewed this week.
 - Once 20–30 details are ready, the set will be balloted and published as an NSBA-only document (not through AASHTO COBS).
- k. TG 15 – Aaron Costin (University of Florida)

- The group continues to collect data in support of an ongoing pooled-fund study.
 - This effort aims to develop a standardized set of digital templates, adapted from European examples, to replace earlier Excel-based formats.
 - These templates will be populated with data as the work progresses.
- l. TG 16 – Sougata Roy (SOCOTEC Engineering, Inc.)
- The task group is developing a slide deck on Orthotropic Steel Decks (OSD) to educate owners and designers.
Potential presentation venues include NSBA Steel Bridge Forums, NASCC, and Movable Bridge Conferences.
Recent presentations included:
 - Frank Artmont: Standard details for open-rib OSD.
 - Casey Rafter (Sika): Polymer polymer-concrete (PPC) wearing surfaces.
A set of OSD standard plans has been submitted to FHWA, though the public release date is not yet known.
- m. TG 17 – Jennifer Pazdon (CAST CONNEX)
- TG17 did not meet this week; Jason Stith provided the update.
The group is working on three priority topics related to custom steel castings:
 - Production welding procedures
 - Design and FEA analysis methods
 - Specialized NDT requirements for acceptance
- n. TG 18 – Jason Provines (VDOT)
- TG18 did not meet in person this week but held a virtual meeting on September 30.
 - Both S18.1 and S18.2 are nearing completion of typesetting.
The group’s current focus is on developing welding and bolting specifications, to be followed by a fabrication specification at a later stage.
 - A draft of the bolting specification, modeled after ASTM A1082, has been completed.

o. TG 19 – George Patton (H&H)

- This was the first meeting for TG19. The discussion focused on defining the group's future direction and distinguishing its work from that of traditional steel bridge task groups.
- Topics include movable bridge design practices, alignment and fit tolerances, and coordination with the NCHRP construction specification update for movable bridges.
- The group emphasized the need to include maintenance-related guidance, particularly for eliminating outdated details common in older movable bridges.
- Their focus will be on the bridge structure itself, not machinery or electrical systems.
- Potential collaboration with AREMA was recommended. However it should be noted that this is an AASHTO committee and AREMA has its own committee.

3. Other Business (2:20 PM – 3:00 PM)

a. [Publication schedule](#)

A survey will be sent out to Task Group Chairs to get an update on

b. Membership / participation discussion

1. Adjourn

Appendix A - Collaboration Document Status

Document	Status	Year Completed/Targeted	Task Group	Task Group Name	Document Title
G1.3.2002	Released	2002	1	Detailing	Shop Detail Drawing Presentation Guidelines
G1.2.2003	Released	2003	1	Detailing	Design Drawing Presentation Guidelines
G1.4.2006	Released	2006	1	Detailing	Guidelines for Design Details
G1.1.2020	Released	2020	1	Detailing	Shop Drawings Approval Review/Approval Guide
G1.3	Update - In-Progress	Unknown	1	Detailing	Shop Detail Drawing Presentation Guidelines
G1.2	Update - In-Progress	Unknown	1	Detailing	Design Drawing Presentation Guidelines
S2.1.2018	Archived	2018	2	Fabrication and Repair	Steel Bridge Fabrication Guide Specification
G2.2.2016	Released	2016	2	Fabrication and Repair	Guidelines for Resolution of Steel Bridge Fabrication Errors
G2.2	Update - In-Progress	Unknown	2	Fabrication and Repair	Guidelines for Resolution of Steel Bridge Fabrication Errors
S4.1.2002	Archived	2002	4	QC/QA	Steel Bridge Fabrication QC/QA Guide Specification
G4.4.2006	Released	2006	4	QC/QA	Sample Owners Quality Assurance Manual
G4.1.2025	Released	2025	4	QC/QA	Steel Bridge Fabrication QC/QA Guidelines
G4.2.2024	Released	2024	4	QC/QA	Guidelines for the Qualification of Structural Bolting Inspectors
G4.4	Update - In-Progress	Unknown	4	QC/QA	Sample Owners Quality Assurance Manual
S4.3	Update - In-Progress	Unknown	4	QC/QA	Specification for Steel Bridge Third Party Quality Assurance
S8.1.2014	Released	2014	8	Corrosion Protection	Guide Specification for Application of Coating Systems
S8.1	Submitted to AASHTO Steel Committee for Comment	2026	8	Corrosion Protection	Guide Specification for Application of Coating Systems
S8.2.2017	Released	2017	8	Corrosion Protection	Thermal Spray Coating Guide
S8.3	Released	2022	8	Corrosion Protection	Galvanizing Guide Specification
G8.4	New - In-Progress	Unknown	8	Corrosion Protection	Detailing for Coatings and Weathering Steel
G9.1	Released	2022	9	Bearings	Steel Bridge Bearing Design and Detailing Guidelines
S10.1.2023	Released	2023	10	Erection	Steel Bridge Erection Guide Specification
G8.X	Submitted to AASHTO Steel Committee for Comment	2027	8	Corrosion Protection	Uncoated Weathering Steel Reference Guide
G10.2	New - In-Progress	2027	10	Erection	Behavior of Steel Bridges during Erection
G11.1	Submitted to AASHTO Steel Committee for Comment	2026	11	Design	Guidelines for the Design of Cross-frame and Diaphragm Members
G12.1.2020	Released	2020	12	Design for Constructability and Fabrication	Guidelines to Design for Constructability and Fabrication
G12.1	Update - In-Progress	Unknown	12	Design for Constructability and Fabrication	Guidelines to Design for Constructability and Fabrication
G12.2	Released	2024	12	Design for Constructability and Fabrication	Guidelines for Steel Bent Caps
G13.1.2019	Released	2019	13	Analysis of Steel Bridges	Guidelines for Steel Girder Bridge Analysis
G13.2	Released	2024	13	Analysis of Steel Bridges	Guidelines for the Analysis of Trusses
G14.1.2021	Released	2021	14	Field Repairs and Retrofits	Maintenance Guidelines for Steel Bridges to Address Fatigue Cracking and Details at Risk of Constraint Induced Fracture
G14.2.2023	Released	2023	14	Field Repairs and Retrofits	Guidelines for Field Repairs and Retrofits of Steel Bridges
G14.3	New - In-Progress	NA	14	Field Repairs and Retrofits	Database of Sample Field Repair and Retrofit Details for Steel Bridges
G15.10	On Hold	NA	15	Data Modeling for Interoperability	BrIM Process Model Definition for Steel Bridge Erection
G15.1	On Hold	NA	15	Data Modeling for Interoperability	Designer/Fabricator Exchange
G16.1	New - In-Progress	Unknown	16	Orthotropic Deck Panels	Guidelines for the Manufacture of Orthotropic Decks and State of Practice
S17.1	New - In-Progress	Unknown	17	Steel Castings	Guide Specification for Cast Steel Connections

Document	Status	Year Completed/Targeted	Task Group	Task Group Name	Document Title
S18.1	Submitted to AASHTO Publishing	2025	18	Duplex Stainless Steel	Guide Specification for Structural Duplex Stainless Steel Bridge Plate Materials
S18.2	Submitted to AASHTO Publishing	2025	18	Duplex Stainless Steel	Guide Specification for Design of Structural Duplex Stainless Steel Bridges
S18.3	New - In-Progress	Unknown	18	Duplex Stainless Steel	Guide Specification for Duplex Stainless Steel - Welding

Appendix B - Member Rosters Unofficial (2026 – 2027)

TG 1 Detailing

First Name	Last Name	Company
Randall	Harrison	W&W AFCO Steel
Domenic	Coletti	HDR
Brad	Dillman	High Steel Structures
Keith	Griesing	Hardesty & Hanover, LLC
Yuying	Hu	MnDOT
Zane	Keniston	QMC Auditing
Frank	Kingston	abs Structural Corporation
Dusten	Olds	HDR
Eric	Rau	HDR
Francesco	Russo	Russo Structural Services
Grant	Schmitz	HDR
Jason	Stith	Michael Baker International
Jonathan	Stratton	Eastern Steel Works, Inc.
Enhui	Tan	Minnesota Department of Transportation
Brian	Watson	HDR
Mike	Wiersch	Stupp Bridge Company
Brian	Wolfe	MDTA
Gary	Wisch	DeLong's, Inc.

TG 2 Fabrication and Repair

First Name	Last Name	Company
Heather	Gilmer	Pennoni
Frank	Adragna	TRC Solutions
Art	Bustos	AISC
Hannah	Cheng	New Jersey DOT
Robert	Connor	Purdue University
Donn	Digamon	Georgia Department of Transportation
Brad	Dillman	High Steel Structures
Jon	Edwards	DOT Quality Services
Jason	Gramlick	California Department of Transportation
Keith	Griesing	Hardesty & Hanover, LLC
Randall	Harrison	W&W AFCO Steel
Jamie	Hilton	KTA-Tator, Inc.
David	Johnson	Industrial Steel Construction, Inc.
Zane	Keniston	QMC Auditing
Jason	Lloyd	Nucor
Kara	Lorenz	High Steel Structures, LLC
Ronnie	Medlock	High Steel Structures
Teresa	Michalk	Texas DOT Material and Tests Div.
Justin	Ocel	Federal Highway Administration
Eric	Rau	HDR
Sougata	Roy	SOCOTEC Engineering, Inc.
Phillip	Sausser	Slim Buttes Structural Engineering Services LLC
Gerard	Sova	Hardesty & Hanover, LLC
Gerard	Sova	Hardesty & Hanover, LLC
Jonathan	Stratton	Eastern Steel Works, Inc.
Brad	Streeter	Scougal Rubber Corporation
Enhui	Tan	Minnesota Department of Transportation
Gary	Wisch	DeLong's, Inc.
Duncan	Paterson	NSBA

TG 4 QC/QA

First Name	Last Name	Company
Jamie	Hilton	KTA-Tator, Inc.
Mark	Alexander	NexGen Contracting
Art	Bustos	AISC
Jose	Capa Salinas	University of St. Thomas
Matthew	Conso	Massachusetts Department of Transportation
Heather	Gilmer	Pennoni
Chad	Hawkins	Infrastructure Consulting and Engineering
Robert	Horwhat	TRC Solutions
David	Johnson	Industrial Steel Construction, Inc.
Zane	Keniston	QMC Auditing
Terry	Logan	Atema, Inc.
Teresa	Michalk	Texas DOT Material and Tests Div.
Anna	Petroski	Atema, Inc.
Shawn	Potter	Contech Engineering
Phillip	Sauser	Slim Buttes Structural Engineering Services LLC
Charles	Smith	Kennedy Fabricating Operations LLC.
Jonathan	Stratton	Eastern Steel Works, Inc.
Brad	Streeter	Scougal Rubber Corporation
Maury	Tayarani	Pennoni
Gary	Wisch	DeLong's, Inc.
Robin	Dunlap	High Steel Structures

TG 8 Corrosion Protection

First Name	Last Name	Company
Johnnie	Miller	KTA-Tator, Inc.
Caroline	Bennett	University of Kansas
Kristen	Blankenship	Carboline
Jeremi	Day	Corrosion Innovations
Jon	Edwards	DOT Quality Services
Pete	Engelbert	Job Safety Associates
Alana	Fossa	American Galvanizers Association
Heather	Gilmer	Pennoni
Jamie	Hilton	KTA-Tator, Inc.
Zane	Keniston	QMC Auditing
Kara	Lorenz	High Steel Structures, LLC
Jennifer	McConnell	University of Delaware
Ronnie	Medlock	High Steel Structures
Teresa	Michalk	Texas DOT Material and Tests Div.
Thomas	Murphy	Modjeski and Masters
Justin	Ocel	Federal Highway Administration
Shawn	Potter	Contech Engineering
Brad	Streeter	Scougal Rubber Corporation

TG 9 Bearings

First Name	Last Name	Company
Michael	Culmo	CHA Consulting, Inc.
Robert	Brantley	STV Incorporated
Domenic	Coletti	HDR
Alina	Davidescu	BSC group
Zane	Keniston	QMC Auditing
Teresa	Michalk	Texas DOT Material and Tests Div.
Sougata	Roy	SOCOTEC Engineering, Inc.
Frank	Russo	Russo Structural Services
Gerard	Sova	Hardesty & Hanover, LLC
Brad	Streeter	Scougal Rubber Corporation
Michael	Sullivan	CME Associates, Inc.
Enhui	Tan	Minnesota Department of Transportation
William	Wan	WSP
Gary	Wisch	DeLong's, Inc.
Ron	Watson	RJ Watson, Inc.

TG 10 Erection

First Name	Last Name	Company
Brian	Witte	Parsons
Brandon	Chavel	AISC
Robert	Cisneros	High Steel Structures
Bret	Clark	Halmar International
Domenic	Coletti	HDR
Douglas	Crampton	Wiss, Janney, Elstner Associates
Saeed	Doust	TYLin
David	Fish	Texas Department of Transportation
Christina	Freeman	FDOT
John	Gast	Consultant
Heather	Gilmer	Pennoni
Nickolas	Haltvick	Minnesota Department of Transportation
Matthew	Hellenthal	Benesch
Todd	Helwig	University of Texas at Austin
Russell	Jeck	Senior Project Manager
Jarret	Kasan	HDR
Natalie	McCombs	HNTB
Ronnie	Medlock	High Steel Structures
Dusten	Olds	HDR
Joshua	Orton	Brasfield & Gorrie, LLC
Frank	Russo	Russo Structural Services
Enhui	Tan	Minnesota Department of Transportation
Allie	Wagner	HNTB
Douglas	Whittaker	Michael Baker International
Brian	Wolfe	MDTA
Jason	Stith	Michael Baker International

TG 11 Design

First Name	Last Name	Company
Brandon	Chavel	AISC
Frank	Artmont	Modjeski & Masters, Inc.
Brian	Atkinson	HNTB
Francisco Javier	Bonachera Martin	Purdue University
Travis	Butz	Burgess and Niple
Nick	Cervo	HDR
Bradley	Dillman	High Steel Structures
Saeed	Doust	TYLin
Thomas	Eberhardt	HDR
David	Fish	Texas Department of Transportation
Barney	Frankl	DOWL
Corey	Greco	Hardesty & Hanover, LLC
Keith	Griesing	Hardesty & Hanover, LLC
Todd	Helwig	University of Texas at Austin
Srinivasa	Kotha	HNTB
Alex	Lim	Oregon Department of Transportation
Natalie	McCombs	HNTB
Bryan	Miller	Pennsylvania Department of Transportation
Deanna	Nevling	HDR
Dusten	Olds	HDR
Joshua	Orton	Brasfield & Gorrie, LLC
Eric	Rau	HDR
Anthony	Ream	HDR
Frank	Russo	Russo Structural Services
Donald	Shaw	Indiana Department of Transportation
Kyle	Smith	GPI
Gerard	Sova	Hardesty & Hanover, LLC
Jason	Stith	Michael Baker International
Brian	Watson	HDR
Donald	White	Georgia Institute of Technology
Brian	Wolfe	MDTA
Domenic	Coletti	HDR

TG 12 Design for Constructability and Fabrication

First Name	Last Name	Company
Russell	Jeck	Senior Project Manager
Frank	Artmont	Modjeski & Masters, Inc.
Allan	Berry	BCC
Travis	Butz	Burgess and Niple
Brandon	Chavel	AISC
Domenic	Coletti	HDR
Bradley	Dillman	High Steel Structures
Gregory	Dunn	Michael Baker International
Heather	Gilmer	Pennoni
Keith	Griesing	Hardesty & Hanover, LLC
Randall	Harrison	W&W AFCO Steel
Todd	Helwig	University of Texas at Austin
Natalie	McCombs	HNTB
Ronnie	Medlock	High Steel Structures
Deanna	Nevling	HDR
Dusten	Olds	HDR
Duncan	Paterson	NSBA
Steve	Percassi	Genesis Structures, Inc.
Eric	Rau	HDR
Anthony	Ream	HDR
Frank	Russo	Russo Structural Services
Kyle	Smith	GPI
Gerard	Sova	Hardesty & Hanover, LLC
Jason	Stith	Michael Baker International
Brian	Watson	HDR
Donald	White	Georgia Institute of Technology
Brian	Witte	Parsons
Brian	Wolfe	MDTA

TG 13 Analysis of Steel Bridges

First Name	Last Name	Company
Deanna	Nevling	HDR
Frank	Artmont	Modjeski & Masters, Inc.
Allan	Berry	BCC
Travis	Butz	Burgess and Niple
Nick	Cervo	HDR
Brandon	Chavel	AISC
Domenic	Coletti	HDR
Douglas	Crampton	Wiss, Janney, Elstner Associates
Saeed	Doust	TYLin
Thomas	Eberhardt	HDR
Christina	Freeman	FDOT
Todd	Helwig	University of Texas at Austin
Natalie	McCombs	HNTB
Dusten	Olds	HDR
Joshua	Orton	Brasfield & Gorrie, LLC
Eric	Rau	HDR
Anthony	Ream	HDR
Kyle	Smith	GPI
Gerard	Sova	Hardesty & Hanover, LLC
Jason	Stith	Michael Baker International
Jeff	Svatora	HDR
Brian	Wolfe	MDTA
Frank	Russo	Russo Structural Services

TG 14 Field Repairs and Retrofits

First Name	Last Name	Company
Kyle	Smith	GPI
Brian	Atkinson	HNTB
Travis	Butz	Burgess and Niple
Domenic	Coletti	HDR
Robert	Connor	Purdue University
Douglas	Crampton	Wiss, Janney, Elstner Associates
Joseph	Esposito	GPI
Heather	Gilmer	Pennoni
Hussam	Mahmoud	Colorado State University
Natalie	McCombs	HNTB
Joshua	Orton	Brasfield & Gorrie, LLC
Phillip	Sauser	Slim Buttes Structural Engineering Services LLC
Brian	Wolfe	MDTA

TG 15 Data Modeling for Interoperability

First Name	Last Name	Company
Aaron	Costin	University of Florida
Jerome	Atchison	abs Structural Corporation
Tom	Beam	High Steel Structures, LLC
Colby	Christensen	HDR
Bradley	Dillman	High Steel Structures
Randall	Harrison	W&W AFCO Steel
Frank	Kingston	abs Structural Corporation
Scott	Lecher	HNTB
Rob	McKenna	HDR
Ronnie	Medlock	High Steel Structures
Phillip	Sauser	Slim Buttes Structural Engineering Services LLC
Jason	Stith	Michael Baker International
Eric	Stone	HNTB
Jonathan	Stratton	Eastern Steel Works, Inc.
Enhui	Tan	Minnesota Department of Transportation
Grant	Schmitz	HDR

TG 16 Orthotropic Deck Panels

First Name	Last Name	Company
Sougata	Roy	SOCOTEC Engineering, Inc.
Frederic	Bergeron	CANAM Bridges
Domenic	Coletti	HDR
Justin	Dahlberg	Iowa State University
Karl	Frank	Consultant
Keith	Griesing	Hardesty & Hanover, LLC
Terry	Logan	Atema, Inc.
Ronnie	Medlock	High Steel Structures
Duncan	Paterson	NSBA
Paul	Tsakopoulos	COWI Consulting, Inc.
Frank	Artmont	Modjeski & Masters, Inc.

TG 17 Steel Castings

First Name	Last Name	Company
Jennifer	Pazdon	Cast Connex
Nicholas	Altebrando	STV Incorporated
Frank	Artmont	Modjeski & Masters, Inc.
Carlos	de Oliveira	Cast Connex
Karl	Frank	Consultant
Heather	Gilmer	Pennoni
Jason	Gramlick	California Department of Transportation
Keith	Griesing	Hardesty & Hanover, LLC
Greg	Hasbrouck	Parsons
Dawn	Lehman	University of Washington
Ronnie	Medlock	High Steel Structures
Thomas	Murphy	Modjeski and Masters
Justin	Ocel	Federal Highway Administration
Sougata	Roy	SOCOTEC Engineering, Inc.
Jason	Stith	Michael Baker International

TG 18 Duplex Stainless Steel

First Name	Last Name	Company
Jason	Provines	Virginia Department of Transportation
Ted	Bush	HDR
Brandon	Chavel	AISC
Gary	Coates	Nickel Institute
Karl	Frank	Consultant
Stan	Gingrich	Amentum
Randall	Harrison	W&W AFCO Steel
Ronnie	Medlock	High Steel Structures
Francisco	Meza	Steel Construction Institute
Rim	Nayal	NuScale Power
Justin	Ocel	Federal Highway Administration
Jennifer	Pazdon	Cast Connex
Juan	Sobrino	Pedelta
Carmen	Vertullo	Carver Labs
Nancy	Baddoo	Steel Construction Institute

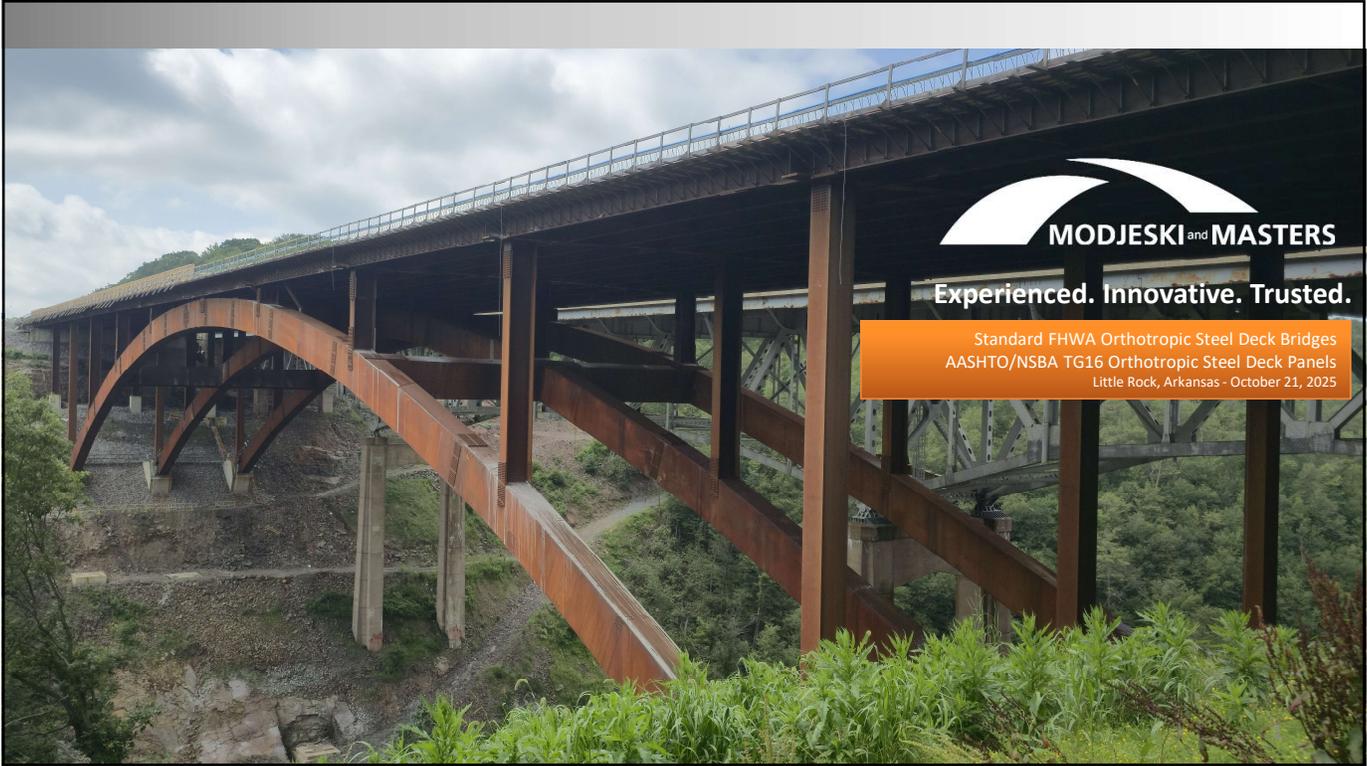
TG 19 Movable Bridges

First Name	Last Name	Company
George	Patton	Hardesty & Hanover, LLC
James	Alison	Steward Machine Co.
Frederic	Bergeron	CANAM Bridges
Domenic	Coletti	HDR
Bret	Gist	G&G Steel
Keith	Griesing	Hardesty & Hanover, LLC
Gregory	Harrell	HNTB
Dale	Ison	Precision Build
Deanna	Nevling	HDR
Felix	Padilla	Florida Department of Transportation
Jim	Phillips	Hardesty & Hanover, LLC
Miguel	Ramirez	Florida Department of Transportation
Todd	Stephens	Modjeski & Masters, Inc.
Jordan	Warncke	HDR
Frank	Artmont	Modjeski & Masters, Inc.

Main Committee

First Name	Last Name	Company
Ronnie	Medlock	High Steel Structures
Frank	Armont	Modjeski & Masters, Inc.
Allan	Berry	BCC
Brandon	Chavel	AISC
Domenic	Coletti	HDR
Aaron	Costin	University of Florida
Michael	Culmo	CHA Consulting, Inc.
Brad	Dillman	High Steel Structures
Karl	Frank	Consultant
Heather	Gilmer	Pennoni
Randy	Harrison	W&W AFCO Steel
Jamie	Hilton	KTA-Tator, Inc.
Russell	Jeck	Senior Project Manager
Johnnie	Miller	KTA-Tator, Inc.
Deanna	Nevling	HDR
Duncan	Paterson	NSBA
George	Patton	Hardesty & Hanover, LLC
Jennifer	Pazdon	Cast Connex
Sougata	Roy	SOCOTEC Engineering, Inc.
Francesco	Russo	Russo Structural Services
Phillip	Sausser	Slim Buttes Structural Engineering Services LLC
Kyle	Smith	GPI
Jason	Stith	Michael Baker International
Jonathan	Stratton	Eastern Steel Works, Inc.
Gary	Wisch	DeLong's, Inc.
Brian	Witte	Parsons
Brian	Wolfe	MDTA
Natalie	McCombs	HNTB

Appendix C – TG16 Additional Meeting Material



1

Background

- 2012 FHWA Guide
 - Has (almost) everything you need to know for all levels of design
 - Less accessible to OSD “newbies”
- 2022 FHWA Guide
 - Focuses on Level 1 Design
 - Contained two optional demonstration tasks

US DEPARTMENT OF TRANSPORTATION
 FEDERAL HIGHWAY ADMINISTRATION

MANUAL FOR DESIGN, CONSTRUCTION, AND
 MAINTENANCE OF ORTHOTROPIC STEEL
 DECK BRIDGES

Publication No. FHWA-IF-12-027
 February 2012

FHWA-HF-22-066 | December 2022
 Federal Highway Administration | 100 New Jersey Ave., SE, Washington, DC 20590

U.S. Department
 of Transportation
 Federal Highway
 Administration

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Optional Demonstration Tasks

- Two tasks, each task for a real bridge project
 - Only one real project was identified
- For second optional task: make family of standard designs
- FHWA through Justin Dahlberg/Iowa State issued the following tasks
 - Task 1: Develop a preliminary design for a short span, two lane OSD bridge
 - Task 2: Develop a family of standard designs for short span OSD bridges
- Started in July 2025, finished in October 2025 (last week!)
- Start with FHWA standard designs, then talk about real life example

3

3

FHWA Standard OSDB Designs - Key Goals

- Modular
 - Panels can be put together side-by-side to achieve the necessary width without changing design
 - Each panel has a welded steel plate girder at (or near its center)
- Repeatable
 - Details are the same between all panels, allowing for manufacturing rather than fabrication
- Versatile
 - Modularity allows for adjustments in width and length (only change is girder depth)
 - Field segments are small, allowing for shipping and hot-dip galvanizing if desired
- Accessible
 - Open rib design means more accessible fabrication (fillet welds!)
 - Steel plate girder superstructure accessible to all designers

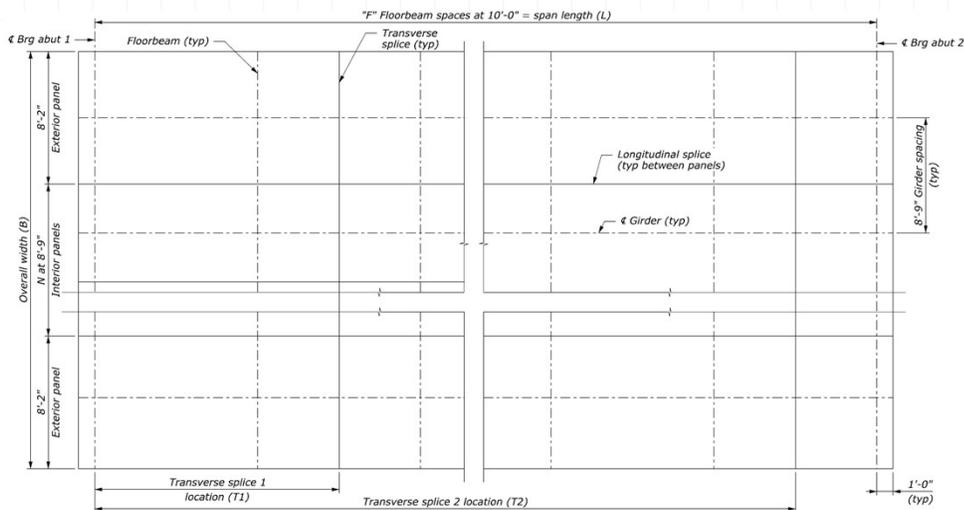
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Standard Design Features

- AASHTO LRFD using HL-93 live load
- Permanent wearing surface included
 - 3" at 150 pcf -> allows for bolted deck plate splices
- Additional future wearing surface (25 psf) also included
- Girder designs use 1.05 redundancy factor for NSTMs in two- or three-girder systems if desired
- All grade 50 steel
- Hot-dip galvanizing friendly!
 - Maximum segment length of ~50 ft
 - Bolted connections designed as Class C
- Steel railing system likely MASH TL-4

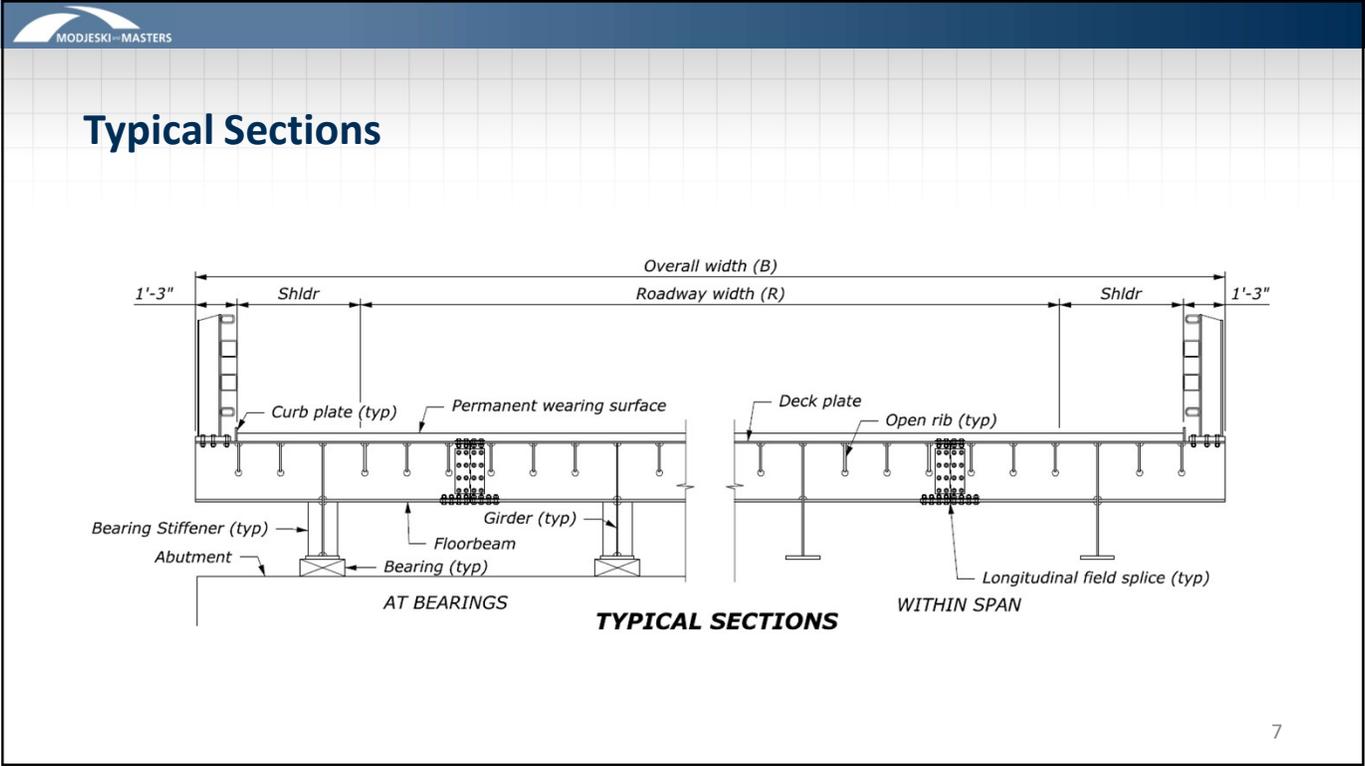
Framing Plan



FRAMING PLAN
(Ribs not shown for clarity)

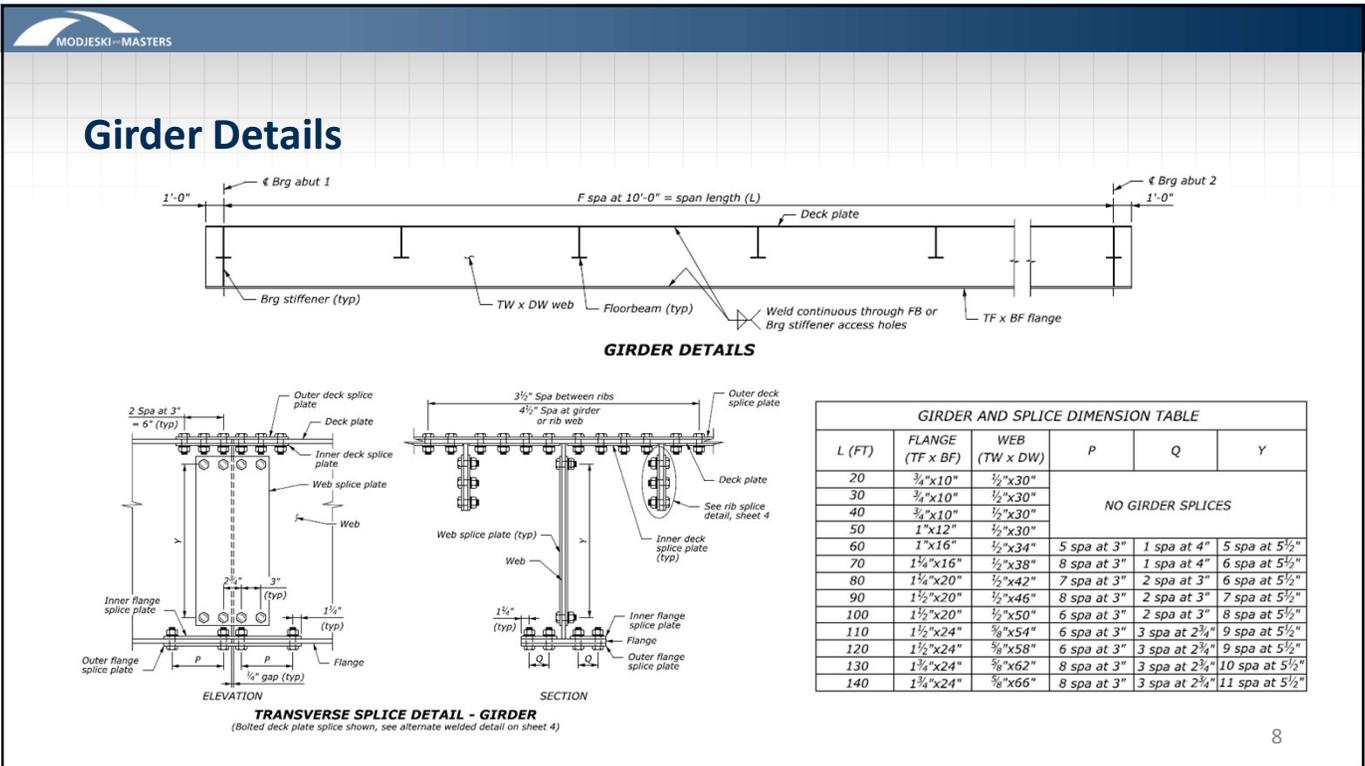
L (FT)	F (EACH)	T1 (FT)	T2 (FT)
20	2	N/A	N/A
30	3	N/A	N/A
40	4	N/A	N/A
50	5	N/A	N/A
60	6	15	N/A
70	7	25	N/A
80	8	35	N/A
90	9	45	N/A
100	10	25	75
110	11	35	75
120	12	35	85
130	13	45	85
140	14	45	95

N (EACH)	B (FT)	R (FT)
0	16'-4"	13'-10"
1	25'-1"	22'-2"
2	33'-10"	31'-4"
3	42'-2"	40'-1"
4	51'-4"	48'-10"
5	60'-1"	57'-3"
6	68'-10"	66'-4"



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MODJESKI—MASTERS

OSD Panel Details

TYPICAL OSDB DETAILS

Labels: 5/8" Deck plate, 5/8"x10" Rib (typ), 1" R (typ), 1/2" (typ), 2" Dia (typ), Floorbeam (typ), GIRDER, Typ, wrap weld through access hole/cope, Finish to bear.

EXTERIOR PANEL - FLOORBEAM DETAIL

Labels: 1'-3", 5/8"x4" Curb plate, Girder web, Deck plate, 1/2"x20" Web (typ), 3/4"x 10" Flange (typ), 3'-9 1/2", 4'-4 1/2", Rib (typ), For cutout details, see sheet 4.

INTERIOR PANEL - FLOORBEAM DETAIL

Labels: Girder web, Deck plate, 1/2"x20" Web (typ), 3/4"x 10" Flange (typ), 4'-4 1/2", Rib (typ), For cutout details, see sheet 4.

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MODJESKI—MASTERS

Railing Details

TYPICAL RAILING DETAIL

Labels: Railing post W8x28, HSS6x6x3/8, L5x5x3/8 Railing angle, HSS5x3x1/2, 1 3/4" x 12 3/4" x 14" Base plate, Curb plate, 7/8" Dia ASTM F3125 Gr F1852 Bolt, Type 1, Galvanized (Typ for bolts on outer surfaces of rails).

- Based on TBTA Railing (FHWA Control No. B-274)
- Crash-tested railing uses 8'-3" spacing and achieved MASH TL-5
- Posts mounted on floorbeams spaced at 10'-0"
- Calculations show likely TL-4

0.000 s

0.400 s

0.800 s

1.200 s

10

10

MODJESKI—MASTERS

Splice Details

LONGITUDINAL SPLICE DETAIL
(Bolted deck plate splice shown, see alternate welded detail, this sheet)

RIB SPLICE DETAIL
(Bolted deck plate splice shown, see alternate welded detail, this sheet)

ALTERNATE WELDED DECK SPLICE DETAILS

Labels in diagrams include: Deck plate (typ), Outer deck splice plate, Inner deck splice plate, Rib (typ), Web splice plate (typ), Inner flange splice plate, Outer flange splice plate, Floorbeam bot flange, Gap, Symm about ϕ splice, 2 5/8", 1/4", 3 spa at 4 1/2", 3 spa at 2 5/8", 1 1/4", 2 Spa at 3" = 6" (typ), 1/4", 2 Spa at 3" = 6", 1 1/4" (typ), CJP, remove backing bar after welding, CJP, backing bar to remain in plate, Bolted web splice, Bolted rib splice, LONGITUDINAL, TRANSVERSE.

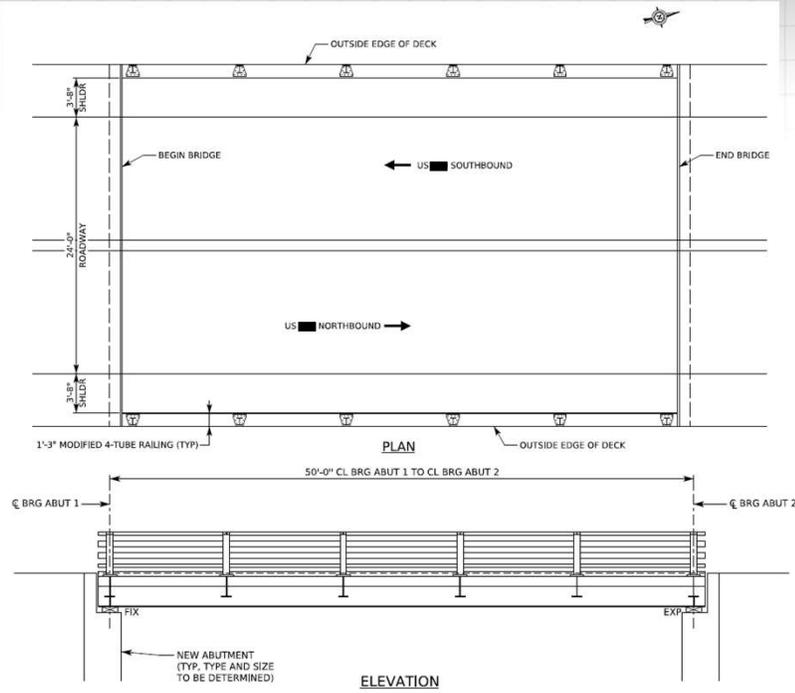
MODJESKI—MASTERS

Now, how to apply to real world?

- Potential (!) project
- 30-foot span with significant skew
- Adjacent concrete box beams with transverse tie rods
- US route in rural area with long detour
- Needs replacement due to condition

Plan and Elevation

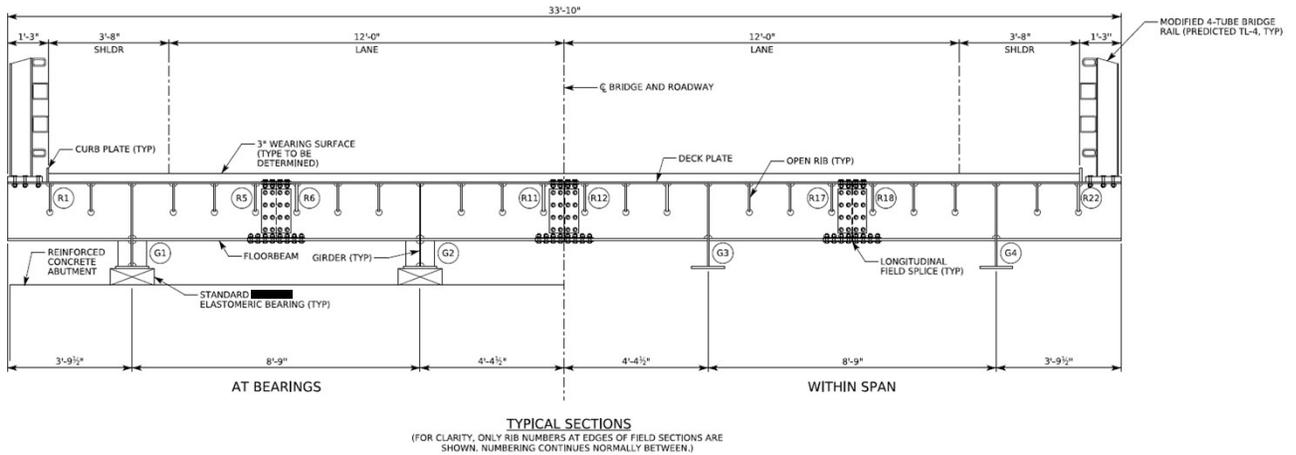
- Increased span to 50 feet to remove skew
- Two lanes at 12 feet
- Shoulders at 3'-8"
- OSD details match those in FHWA standard plans



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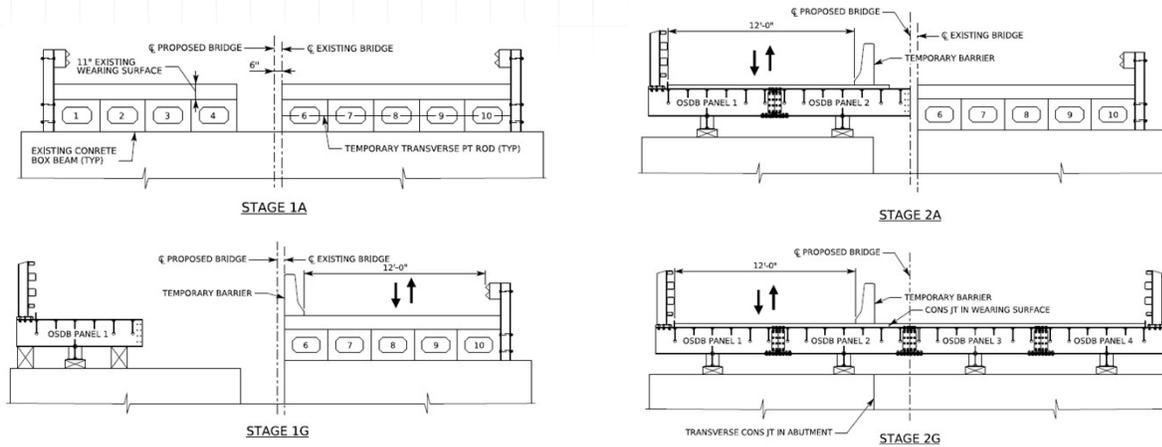
Elevation and Typical Sections



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Construction Sequence



- Maintain bi-directional traffic over single lane with limited full closures

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Conclusions

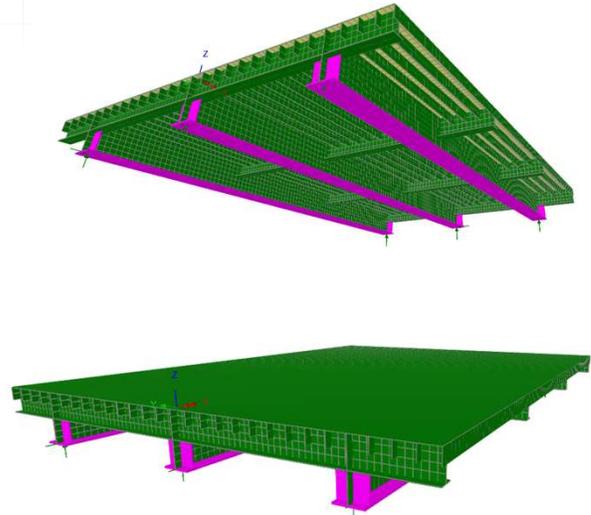
- Standardization and modularity
 - FHWA standard OSDB designs offer a modular, repeatable, and versatile solution for short-span bridges, making them accessible for a wide range of designers and manufacturers
- Ease of fabrication and installation
 - Open rib design and standardized details facilitate manufacturing, shipping, and hot-dip galvanizing
- Improved accessibility
 - Approach lowers barriers for new designers and streamlines the design and construction process for shot span OSDBs
- Real-world applicability
 - Potential demonstration project shows that standard designs can be adapted to real-world scenarios, such as rural bridge replacements

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Next Steps

- Standard designs all preliminary
 - Weld sizes not designed
 - Splice plate thicknesses assumed
 - Fatigue checked only for global details
- Check fatigue details and design
 - Level 1 means should be okay, but would need to verify before anything being built
- Verify 1D design assumptions through modeling
 - Effective width, distribution factors, etc.



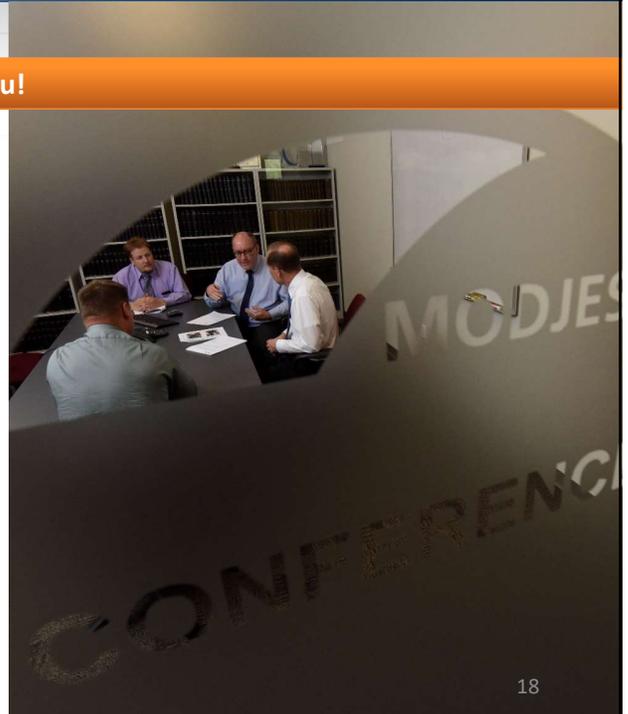
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Contact Information

- **Frank A. Artmont, PhD, PE**
Senior Engineer | National Bridge Group
 100 Sterling Parkway, Suite 302
 Mechanicsburg, PA 17053
FAArtmont@modjeski.com

Thank You!



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POLYESTER POLYMER CONCRETE WEARING SURFACES FOR ORTHOTROPIC STEEL DECKS

10/21/25, CASEY RAFTER

KWIK BOND POLYMERS, a SIKA Company



BUILDING TRUST



KWIK BOND POLYMERS PRODUCT OFFERING

High Molecular Weight Methacrylate (HMWM)
Polyester Polymer Concrete (PPC)
Hybrid Composite Synthetic Concrete (HCSC)
Thin Polymer Overlay Advanced (TPO AD)
High Friction Surface Treatment (HFST)



BUILDING TRUST



KWIK BOND POLYMERS

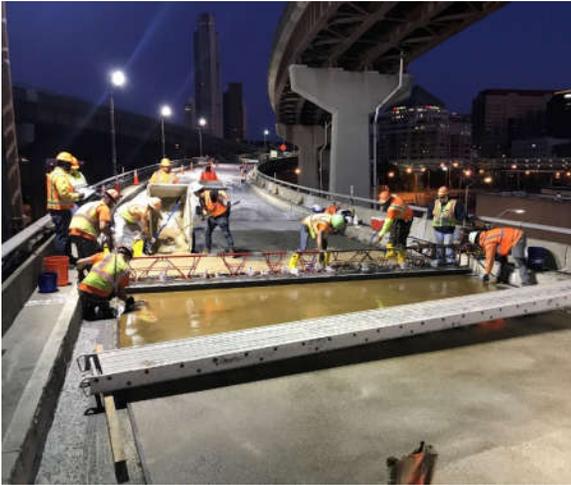
POLYESTER POLYMER CONCRETE

- PPC is a non-cementitious, polymer concrete installed like regular concrete
- Primary application is bridge deck overlay for preservation and rehabilitation
- Thousands of Joint Headers & Full Depth Joints
- Thousands of patches, partial to full
- Some closure pours (all successful)
- Overlays on Grid and Orthotropic Steel Decks
- >40 years of proven history
- >120,000,000 SF Bridge Deck Area nationwide



POLYESTER POLYMER CONCRETE HISTORY & DEVELOPMENT

- PPC development began in 1960's in California
- Caltrans and Oregon were leaders during trial period
- The same resins and aggregates used back then are used today
- Kwik Bond Polymers has direct lineage from the 1970's to today



POLYESTER POLYMER CONCRETE HISTORY & DEVELOPMENT

Studies Leading to Choice of Epoxy Asphalt for Pavement on Steel Orthotropic Bridge Deck of San Mateo-Hayward Bridge

BEN BALALA, California Division of Bay Toll Crossings

Long-span bridges with orthotropic steel decks have created the need for a lightweight, durable surfacing to act as both a leveling course and pavement. The pavements used by the originators of orthotropic steel deck plate girders in Europe are not feasible for use in this country. Developments in synthetic resin pavements show promise. The problem, insofar as available materials are concerned, is related to overlays used to repair damaged portland cement concrete bridge decks.

The experiences of the California Division of Bay Toll Crossings on major toll bridges in the San Francisco Bay Area are related. These include choice of a thin epoxy coal tar overlay, $\frac{1}{8}$ in. to $\frac{1}{16}$ in. thick on the San Francisco-Oakland Bay Bridge concrete decks, and choice of an epoxy asphalt concrete pavement, $1\frac{1}{2}$ in. to $2\frac{1}{2}$ in. thick on the steel orthotropic deck of the San Mateo-Hayward Bridge. The first epoxy coal tar was experimentally applied to the San Francisco-Oakland Bay Bridge in 1958. Subsequent studies progressively testing over 20 materials are still in progress.

The author believes that when numerical criteria have been established various resins may be satisfactory if acceptable application methods can be developed. A clearinghouse for accumulation of experience on the subject is required. Experimental applications are needed. The methods for measuring adhesion in direct tension on a diamond-drill cut core and fatigue in bending are mentioned as a start on the problem of establishing numerical criteria.

*LONG-SPAN bridges with orthotropic steel decks have created the need for a lightweight, durable surfacing to act as both leveling course and pavement. A variety of solutions to this problem by the originators of this type of construction in Europe are either not feasible or not permanent enough for recently projected uses. Developments in synthetic resins show promise in solving this problem. Earlier studies for concrete bridge deck overlays gave some insight into the area of resinous pavements.

The qualitative criteria developed for the intended use were investigated for various materials and choice made for the San Mateo-Hayward Bridge. Continuing developments and the results obtained in both testing laboratories and actual installations will probably lead to innovations in the use of synthetic resins for this purpose.

The history of construction of orthotropic steel deck bridges and the history of research into pavements for orthotropic steel decks in general are well covered (4, 5, 9).

Paper sponsored by Committee on Adhesives, Bonding Agents and Their Uses and presented at the 48th Annual Meeting.

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good condition but it was necessary to obliterate the tile markers, which were slightly raised above the surface of the concrete in order to change the traffic pattern.

Studies at this time evaluated moduli of elasticity, coefficient of expansion, and adhesion for a number of aggregate-filled resins as well as for latex modified portland cement concrete.

The subject of resins had been broached to the Division of Bay Toll Crossings in 1958 by a test application of Guardkote 140 on the San Francisco-Oakland Bay Bridge upper deck with the cooperation of the Shell Chemical Company. Guardkote 140 was an epoxy coal tar formulation derived from basic patents held by the Pittsburgh Coke and Chemical Company.

At about this same time we were approached by the California Chemical Company, Oronite Division of Standard Oil Company of California, regarding use of a polyester resin for this purpose. The possibility of a polyester performing the same function as an epoxy at about half the cost sounded attractive. A further attraction was the fact that although the epoxies were truly two component materials requiring intimate mixing and precise proportioning, the polyesters were catalyzed only and less critical mixing would still produce the required end product.

Test installations of five materials each about 20 ft long and about 12 ft wide were placed on the lower deck of the San Francisco-Oakland Bay Bridge in 1962. There were two latex-modified concretes, three polyester resins, an epoxy asphalt, and a proprietary concrete floor system without an adhesive (2). The epoxy asphalt formulation used in this application never seemed to set up, and abraded quickly under the heavy traffic. The proprietary concrete floor system and the latex-modified concretes showed under hand hammer soundings, extensive ratty areas indicating general lack of bond. The three polyester resins were excellent. The only apparent difficulty or obvious drawback to the polyester resin applications was lack of a commercial method producing an acceptable riding surface.

It became necessary to terminate the test when the lower deck paving contract was awarded in 1964. All test areas other than the polyester resins were readily cleaned down to the original concrete deck which was the new unsurfaced lightweight concrete over the former interurban trackway. It was practically impossible to remove the polyesters without removing part of the concrete substrate, and they were covered by the new surfacing.

The surfacing chosen for the upper deck paving contract in 1963 and the lower deck in 1964 on the basis of cost, commercial quality of application equipment and material, convenience to traffic, and current availability of contractors and equipment was Shell Guardkote 140 (basically a flood coat of epoxy coal tar filled with clean, hard sand passing a number 10 screen), at that time under the control of Shell Chemical Company. This was not a perfect solution but with the state of knowledge at that time it fulfilled most requirements. It obliterated the tile markers satisfactorily, renewed the surface, obliterated the difference in texture between the new and old concrete slabs on the lower deck, and provided a construction method that was compatible with the complicated lane-scheduling procedure required to switch traffic from mixed bidirectional traffic on each deck to unidirectional mixed traffic on each deck. It did not, however, provide a new screeable surface since the placing procedure is somewhat similar to that for a seal coat in that it repeats to some degree the imperfections of the underlying pavement.

In addition, we became acquainted with the capabilities of resin producers and their statements, which we have no reason to doubt, that if we could tell them the physical characteristics of the material required for our use, they could produce it. Numerical criteria developed by future tests may yet produce an opportunity for the resin producers to fulfill their promises.

Shell representatives in 1962 also described their Epon asphalt system, but the half-inch average thickness proposed for the San Francisco-Oakland Bay Bridge due to weight limitations was not considered feasible for Epon asphalt, basically a $\frac{1}{8}$ -in. maximum asphalt-concrete aggregate mixture bound with an epoxy-asphalt compound.

There were countless products investigated that did not receive complete study due to lack of proper financial or technical backing by the vendor. A definite factor in deciding on a coal tar epoxy for the San Francisco-Oakland Bay Bridge was the furnishing of a bonded written guarantee for three years.

- 1969 study for San Mateo-Hayward OSD wearing surface included Polyester Concrete and Epoxy Asphalt Concrete.

- “The only apparent difficulty or obvious drawback to the polyester resin was lack of a commercial method producing and acceptable riding surface.”



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POLYESTER POLYMER CONCRETE PRODUCT OVERVIEW

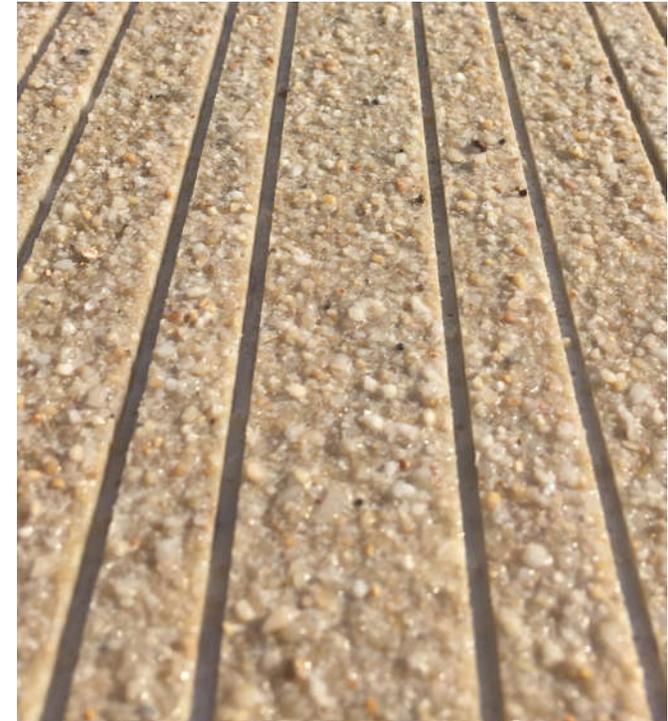
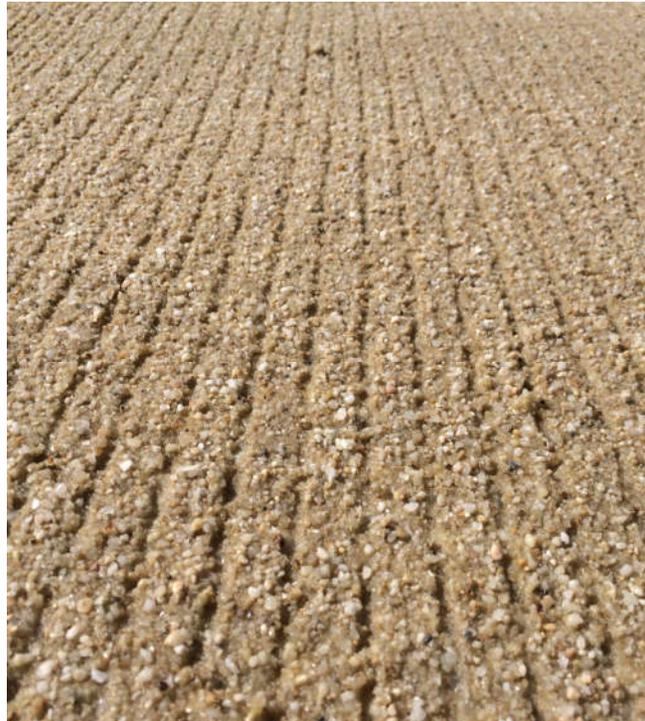
- Components
 - HMWM Primer
 - Graded Silica Aggregate
 - Polyester Resin Binder
 - Abrasive Top Sand
 - **No cement or water**



POLYESTER POLYMER CONCRETE PRODUCT OVERVIEW

■ Properties

- 6,000 psi Compressive
- 800 psi Tensile
- 1,500 psi Flexural
- 1,500 ksi MOE
- 0 coulombs permeability
- Similar CTE to PCC



POLYESTER POLYMER CONCRETE APPLICATIONS & **ADVANTAGES**

- Bridge Deck Overlays
 - ABC Closure Pours
 - Full-depth Patching
 - Full-depth Joints
 - Joint Headers
 - Grade Correction
- Any thickness >3/4"
- 40-100 °F
- 2-hr traffic return always
- 0 coulombs permeability
- 35+ year proven service



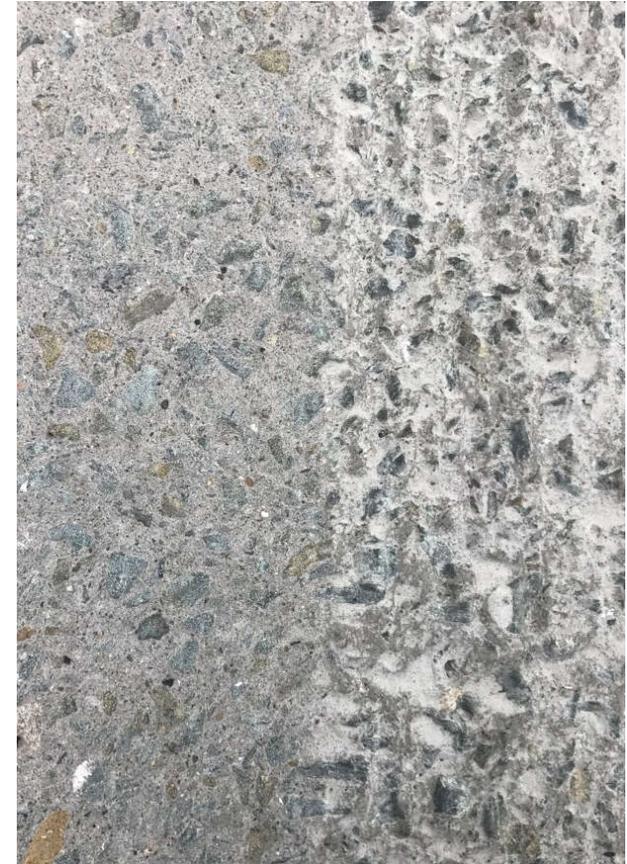
POLYESTER POLYMER CONCRETE INSTALLATION

- Equipment
 - Shot Blaster
 - Volumetric Mixing Truck
 - Slip Form Paver
- Sequence
 - Surface Preparation
 - Install HMWM Primer
 - Catalyze & Mix PPC
 - Place and Finish



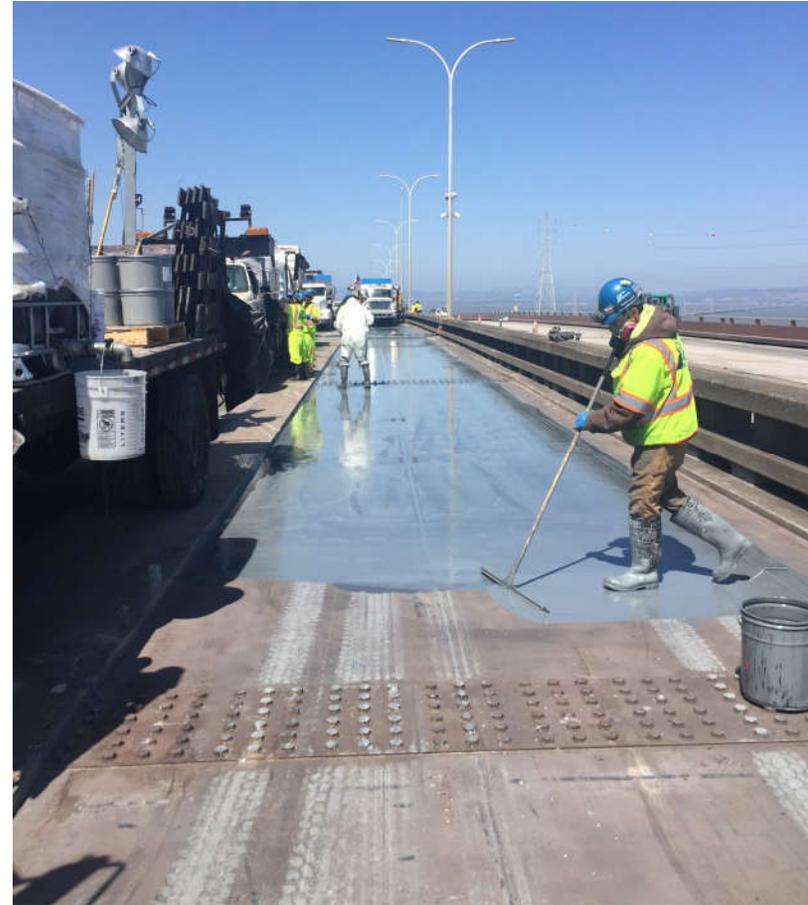
POLYESTER POLYMER CONCRETE INSTALLATION

- Surface Preparation
 - Remove existing overlay
 - Using a Shot Blaster:
 - Clean
 - Sound
 - Visibly Dry



POLYESTER POLYMER CONCRETE INSTALLATION

- Install HMWM Primer
 - Confirm deck temp is 40-100 F
 - Catalyze HMWM in buckets
 - Install with brooms/rollers
 - 100 SF/Gal
- (Zinc added to HMWM for OSD as sacrificial anode)



POLYESTER POLYMER CONCRETE INSTALLATION

- Catalyze & Mix PPC
 - Volumetric mixer truck
 - Hopper for Aggregates
 - 500-gal Tote for Polyester Resin
 - 10-gal containers for MEKP & ZC
 - Calibrated to PPC spec
 - Continuous auger mixes PPC
 - Computer print-out provides weights for pay item



POLYESTER POLYMER CONCRETE INSTALLATION

- Place & Finish
 - Slip Form Paver
 - Distributes PPC material
 - Vibrates material as needed
 - Sets material to grade
 - Controls surface smoothness
 - Hand Finishing
 - Edges & touch-ups
 - Top Sand
 - Hand broadcasted
 - Texturing
 - Tines or saw-cut grooving



WEARING SURFACES FOR ORTHOTROPIC STEEL DECKS



Watson
Bowman
Acme

KWIKBOND
POLYMERS

KING

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OSD WEARING SURFACE OPTIONS

- Option #1 – Thin Polymer Concrete
- Option #2 – Cementitious Concretes
- Option #3 – Asphalt and Modified Asphalt (EAC)
- Option #4 – Thick Polymer Concrete



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OSD WEARING SURFACE OPTIONS

- ~~Option #1 – Thin Polymer Concrete~~
- Option #2 – Cementitious Concretes
- Option #3 – Asphalt and Modified Asphalt (EAC)
- Option #4 – Thick Polymer Concrete

- **Thin Polymer Concrete**
 - Advantages
 - Less costly
 - Fast install
 - No pot-holes
 - Low permeability
 - Disadvantages
 - Does not stiffen composite deck
 - Adhesion issues
 - Wears quickly
 - Shorter service life
 - Thin placements only (<5/8" typically)



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OSD WEARING SURFACE OPTIONS

- ~~Option #1 – Thin Polymer Concrete~~
- ~~Option #2 – Cementitious Concretes~~
- Option #3 – Asphalt and Modified Asphalt (EAC)
- Option #4 – Thick Polymer Concrete

- **Cementitious Concretes**
 - Advantages
 - More familiar
 - Static MOE
 - Significant stiffening capability
 - Disadvantages
 - Requires shear studs
 - Prone to cracking
 - Poor adhesion to steel deck
 - High dead load
 - High cost
 - High permeability



OSD WEARING SURFACE OPTIONS

- ~~Option #1 – Thin Polymer Concrete~~
- ~~Option #2 – Cementitious Concretes~~
- Option #3 – Asphalt and Modified Asphalt (EAC)
- Option #4 – Thick Polymer Concrete

■ Regular Asphalt

- Advantages
 - More familiar
 - Inexpensive
 - Fast install
- Disadvantages
 - Ruts and shoves
 - Does not stiffen composite deck
 - Shorter service life
 - High permeability
 - Higher dead load
 - Very temperature sensitive in service

■ Epoxy Asphalt Concrete

- Advantages
 - Proven performance history
 - Low permeability
 - Good compatibility with OSD
 - Stiffens composite deck
 - Resists rutting and shoving
- Disadvantages
 - Difficult to produce
 - Extended cure times (Up to multiple days/weeks)
 - Inaccessible to some locations
 - Somewhat temperature sensitive in service
 - Small construction window due to temperature

OSD WEARING SURFACE OPTIONS

- ~~Option #1 – Thin Polymer Concrete~~
- ~~Option #2 – Cementitious Concretes~~
- Option #3 – Asphalt and Modified Asphalt (EAC)
- Option #4 – Thick Polymer Concrete

- **Thick Polymer Concrete (Polyester Polymer Concrete)**
 - Advantages
 - Proven Performance History
 - 0 coulombs permeability
 - Rapid install
 - Wider construction window
 - HMWM primer = excellent adhesion to steel
 - Less temperature sensitive during service
 - Stiffens deck greater than Asphalt/EAC
 - Cannot rut or shove
 - High abrasion resistance
 - Disadvantages
 - Shorter service life history
 - Less familiarity in OSD markets
 - Stiffens deck less than cementitious overlay + shear studs



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POLYESTER POLYMER CONCRETE FOR ORTHOTROPIC STEEL DECKS

Evaluation of Wearing Surface Systems for the Orthotropic Steel Deck of the San Mateo Hayward Bridge



Final report prepared for the
California Department of Transportation
Project 59A0742, Contract Manager: Ric Maggenti

Vellore S. Gopalaratnam, Ph.D., P.E.
Professor of Civil Engineering
Ravi Sankar Chamarthi, M.S.
Department of Civil and Environmental Engineering
University of Missouri-Columbia

Report No.: MU Gopalaratnam 12-02
December 2012



University of Missouri-Columbia

STATE OF CALIFORNIA DEPARTMENT OF TRANSPORTATION
TECHNICAL REPORT DOCUMENTATION PAGE

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9. PERFORMING ORGANIZATION NAME AND ADDRESS Department of Civil and Environmental Engineering University of Missouri-Columbia E2509 Lafferre Hall Columbia, Missouri 65211-2200			8. PERFORMING ORGANIZATION REPORT NO. MU Gopalaratnam 12-02
12. SPONSORING AGENCY NAME AND ADDRESS California Department of Transportation Division of Engineering Services 1801 30th Street, Mail Stop 9-2/51 Sacramento, California 95816-0001			10. WORK UNIT NUMBER
15. SUPPLEMENTAL NOTES Prepared in cooperation with the State of California Department of Transportation.			11. CONTRACT OR GRANT NUMBER Contract No. 59A0742
16. ABSTRACT Performance under static and fatigue loads are evaluated for two different wearing surfaces for possible use on the steel orthotropic steel deck of San Mateo Hayward Bridge. The two wearing surface materials studied include a 2" thick (nominal) premixed polyester concrete (PC) and a 2" thick (nominal) epoxy asphalt concrete (EAC). Tests on flexural specimens that comprise a "steel-plate - wearing surface" composite were conducted at several temperatures in the range 20°F - 120°F (in approximately 10°F increments) and at several different dynamic loading frequencies (0.0167, 1.0, 2.5, 5.0, 7.5, 10.0 and 15.0 Hz). Following these tests, fatigue tests were conducted on replicate EAC and PC composite specimens at each of room (70°F), cold (32°F) and hot (120°F) temperatures. Fatigue tests were conducted using sinusoidal loading at a 10 Hz frequency. Maximum loads used in the tests were more severe than design service loads and were computed based on an idealized analysis of transverse bending of the orthotropic deck. Companion investigations that provided significant support data for the evaluation included static flexural and static failure tests, tensile pull-out tests, post-test crack inspection and mapping, and resistivity tests. Effect of composite action and its implications to fatigue performance of the orthotropic steel deck as well as the wearing surface are detailed in the context of variations in the elastic modulus of the wearing surface as a function of temperature and rate of loading. Both the wearing surface systems performed well at the cold temperatures, surviving 10 million fatigue cycles without any cracking or other types of deterioration (slip, debonding, and delamination) at maximum fatigue load levels that are significantly more severe than design service loads. Both wearing surfaces experienced cracking at the room and hot temperatures. Even while cracking occurred well within the limiting 10 million fatigue cycles, when tests on cracked specimens were carried out to the full 10 million fatigue cycles, these cracks did not result in wearing surface delamination or local debonding. In most instances these cracks were not visible in an unloaded state. Even while the service loading may be lower than those used in these fatigue test, cracking is likely in the service performance of both EAC and PC wearing surface materials and it is prudent to have a crack maintenance program in place.			13. TYPE OF REPORT AND PERIOD COVERED Final Report 11/05/2010 - 05/20/2012
17. KEY WORDS Composite Action, Dynamic Behavior, Epoxy Asphalt Concrete, Fatigue Behavior, Fatigue Testing, Polyester Concrete, San Mateo Hayward Bridge, Static Behavior, Thermal Response, Wearing Surface			14. SPONSORING AGENCY CODE
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PPC FOR ORTHOTROPIC STEEL DECKS

SAN MATEO HAYWARD BRIDGE

- U of MC Research
 - Tests on flexural specimens that comprise a “steel plate-wearing surface” composite
 - Polyester Polymer Concrete (2”)
 - Epoxy Asphalt Concrete (2”)
 - Conducted at several temperatures from 20 – 120°F
 - Performed at several dynamic loading frequencies (0.0167, 1, 2.5, 5, 7.5, 10 and 15 Hz)
 - Fatigue tests to replicate EAC and PPC – steel composites at cold, room and hot temps using sinusoidal loading @ 10 Hz
 - Tensile pull-out, crack mapping and resistivity testing



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PPC FOR ORTHOTROPIC STEEL DECKS SAN MATEO HAYWARD BRIDGE

AASHTO LRFD Bridge Design Specifications related to orthotropic steel deck (OSD) bridges as detailed below.

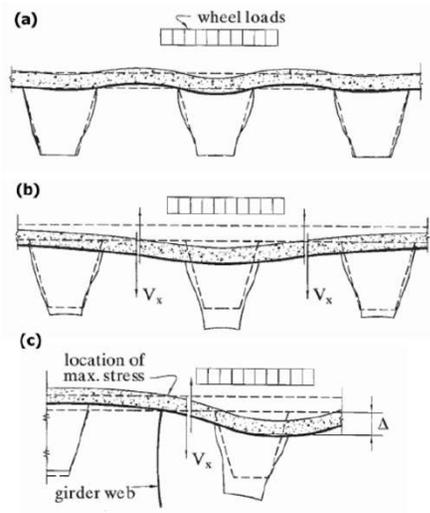


Fig. 2.1 Flexural response and shear forces on the wearing surface-steel composites caused by relative displacements and transverse bending. (a) Closer to floor beams (b) Midway between the floor beams (c) Near the main girder (Wolchuck, 2002)

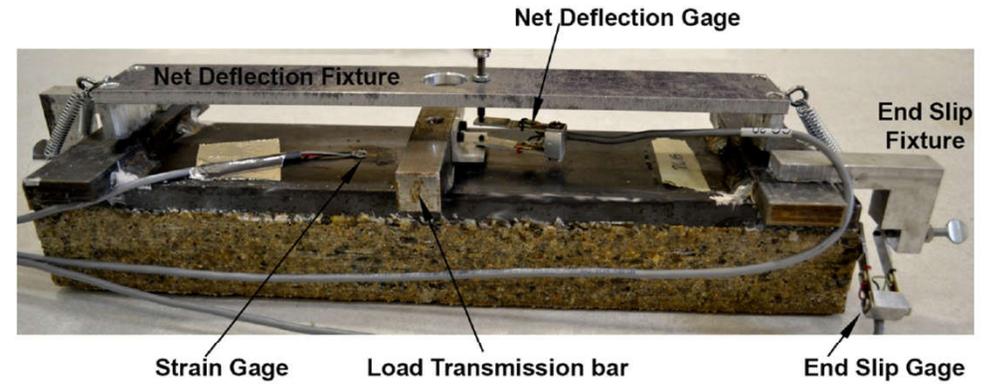


Fig. 3.5 Composite specimen with displacement measurement and loading fixtures attached

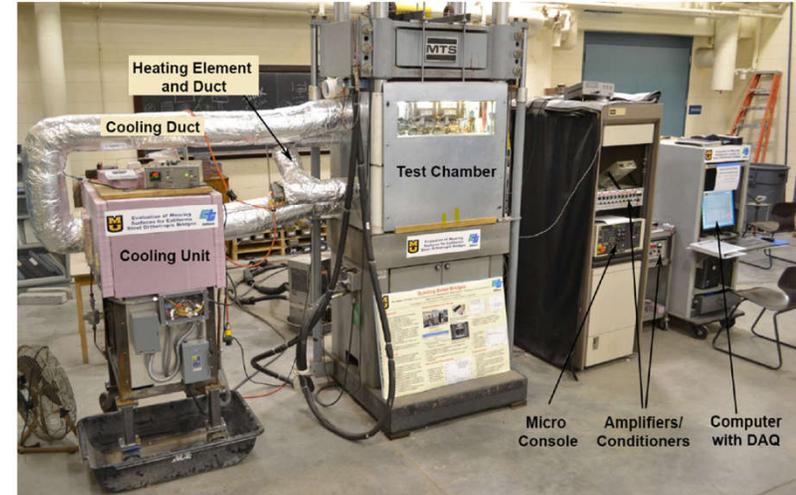


Fig. 3.15 Overall fatigue test set-up

PPC FOR ORTHOTROPIC STEEL DECKS SAN MATEO HAYWARD BRIDGE

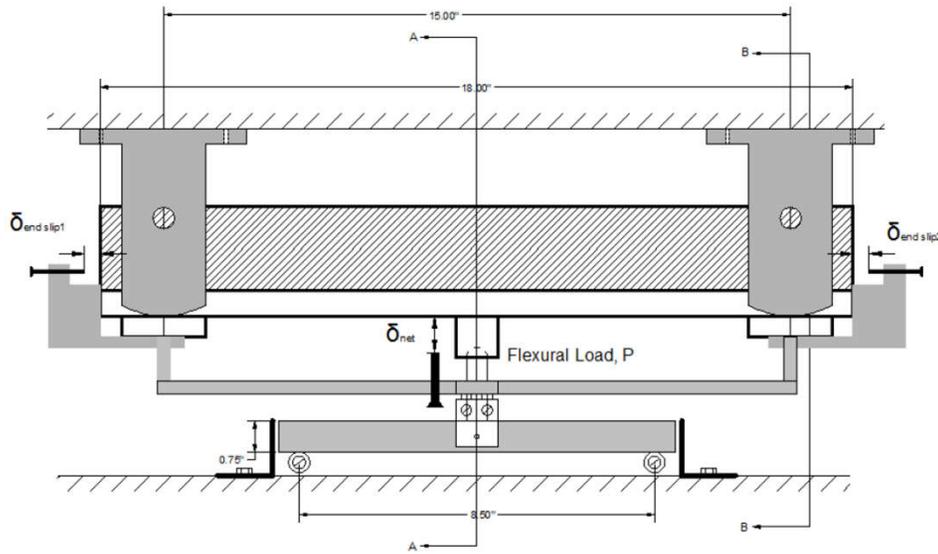


Fig. 3.17 Schematic of the flexural test configuration (see sections AA and BB in Fig. 3.18)

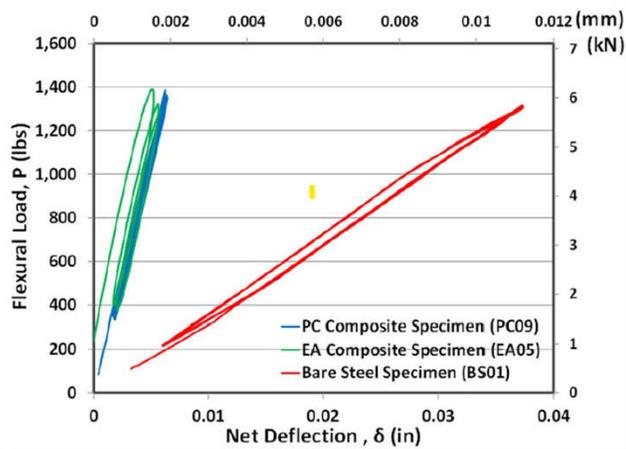


Fig. 3.23

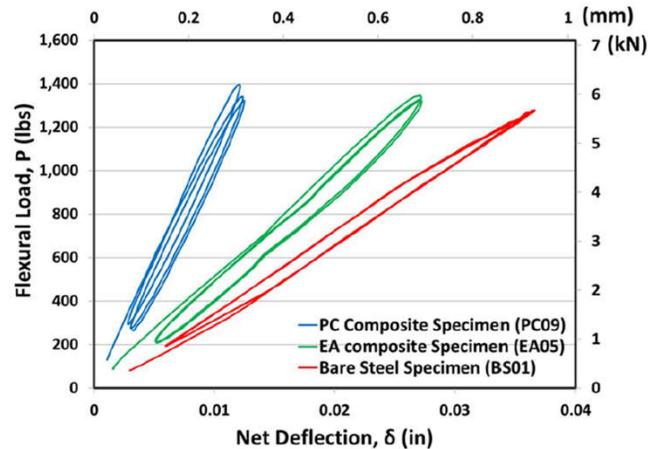
(a) Set-up with top steel plate and other fixtures used for the static failure tests (b) MTS machine used for static failure tests

PPC FOR ORTHOTROPIC STEEL DECKS

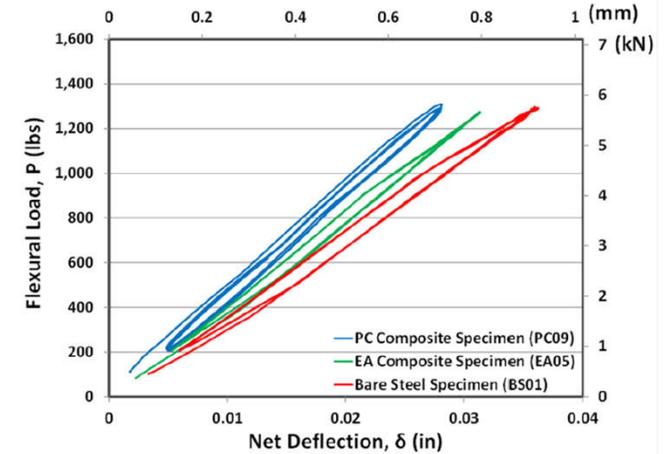
SAN MATEO HAYWARD BRIDGE – STATIC LOAD DEFLECTION



Static load-deflection responses for bare steel and composite specimens temperature (Nominal 32°F)



Static load-deflection responses for bare steel and composite specimens at temperature (Nominal 70°F)



Static load-deflection responses for bare steel and composite specimens at temperature (Nominal 120°F)

- COLD 32°F

- ROOM 70°F

- HOT 120°F

- Static load deflection responses at various temperatures
- Both PPC and EAC are *viscoelastic*, but PPC is stiffer than EAC

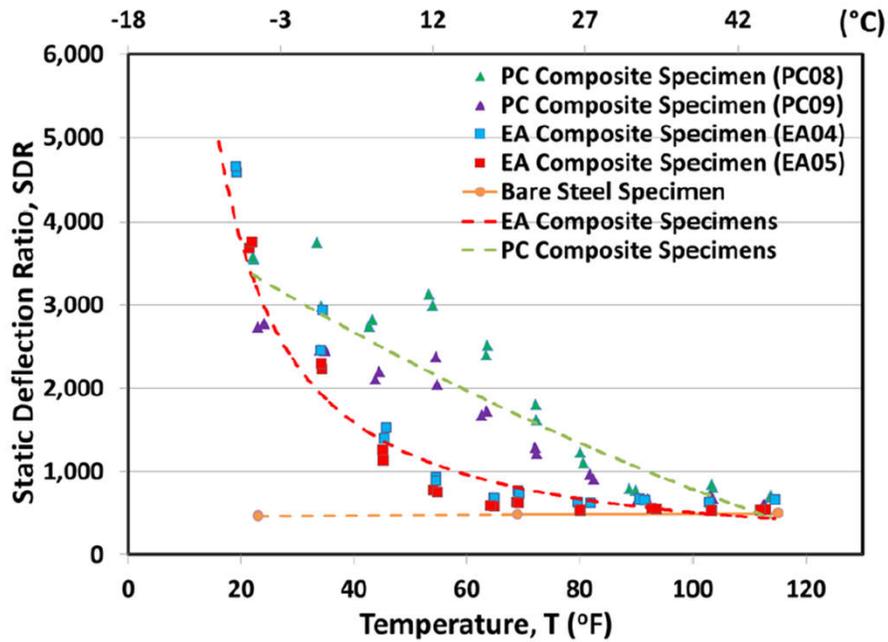


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PPC FOR ORTHOTROPIC STEEL DECKS

SAN MATEO HAYWARD BRIDGE – STATIC LOAD DEFLECTION

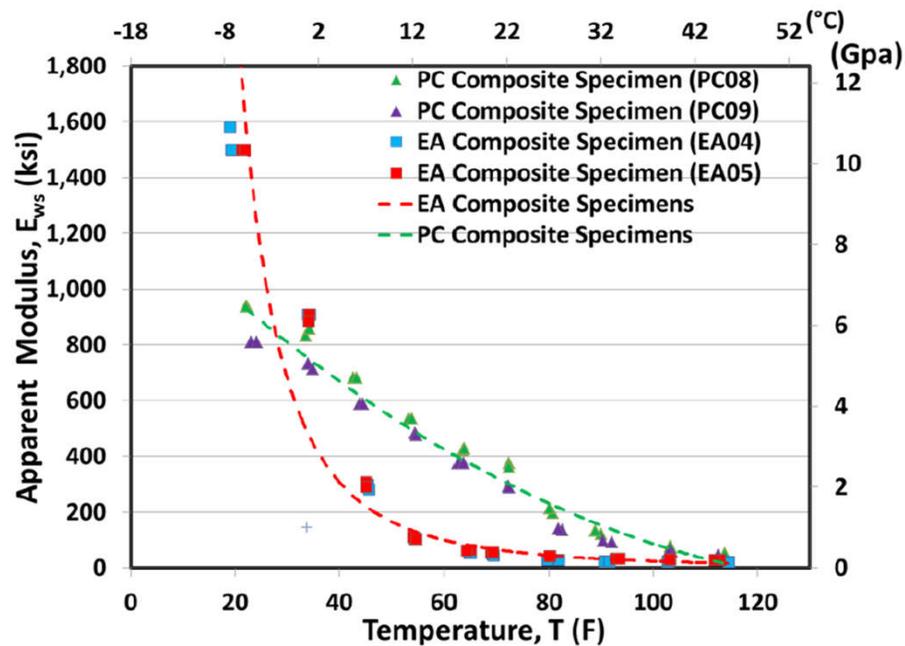


- In the temperature range of 30-80°F, PPC composites exhibit SDR values of 2-4 times higher than the EAC composite specimens

Fig. 5.4 Static deflection ratio of wearing surfaces and bare steel specimens

PPC FOR ORTHOTROPIC STEEL DECKS

SAN MATEO HAYWARD BRIDGE – STATIC LOAD DEFLECTION



- In the 60-80°F temperature range, the apparent elastic modulus of PPC is approximately 6-8 times that of EAC

Apparent elastic modulus as a function of wearing surface temperature from composite EA and PC specimens.

PPC FOR ORTHOTROPIC STEEL DECKS SAN MATEO HAYWARD BRIDGE – PULL-OFF TESTING

Table 5-7 Summary of results from the tensile pull-out tests

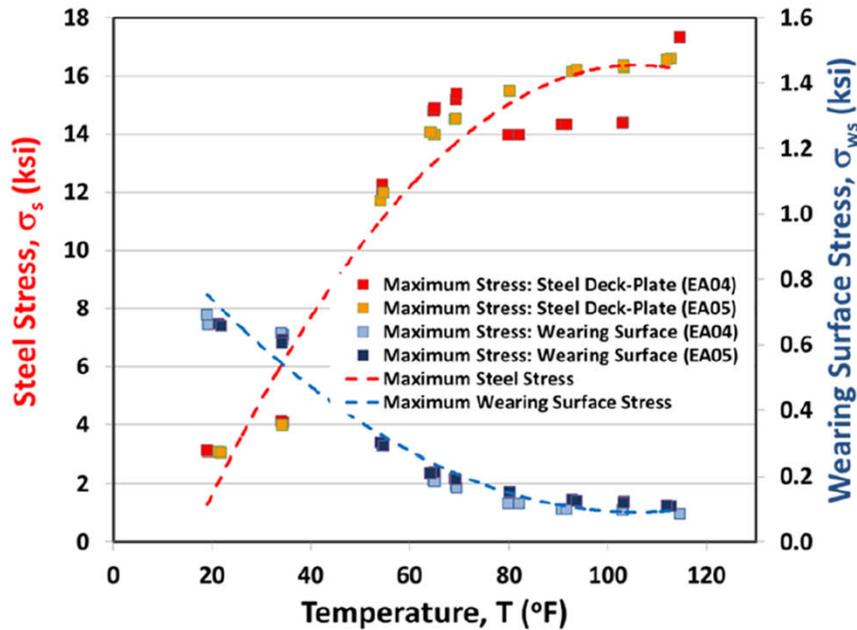
Spec. No.	Core ID	Maximum Load (lbs)	Bond Strength ¹ (psi)	Temp. (°F)	Failure Type	Bonding Agent	Additional Modifications
EA01	A	937	298	75	1, 2, 3 ²	Devcon 5 Min	Wedge Anchor
EA01	B	1,089	347	75	1, 2, 3 ²	Transpo T41	Sleeve Anchor
EA01	C	1,105	352	75	1, 2, 3 ²	Transpo T41	Sleeve Anchor
EA01	D	1,334	425	75	1, 2, 3 ²	Transpo T41	9 Holes ³
EA01	E	1,779	567	75	1, 2, 3 ²	Loctite HD	None
EA01	F	1,672	532	75	3	Loctite MC	None
EA02	B	2,008	639	75	4 ⁴	Loctite HD	Bolt Anchor
EA02	F	1,892	603	75	4 ⁴	Loctite HD	Bolt Anchor
PC06	A	3,730	1,188	32	5	Transpo T41	None
PC06	B	2,433	775	32	1, 2, 3 ²	Transpo T41	None
PC07	B	2,667	849	32	1, 2, 3 ²	Transpo T41	None
PC07	F	2,789	888	32	1, 2, 3 ²	Transpo T41	None
PC06	C	3,102	988	75	5	Loctite MC	None
PC06	D	3,036	967	75	1, 2, 3 ²	Loctite MC	None
PC06	E	3,137	999	75	5	Loctite MC	None
PC06	F	1,397	445	122	5	Transpo T41	None
PC07	A	886	282	122	1, 2, 3 ²	Transpo T41	None
PC07	C	1,335	425	122	5	Transpo T41	None
PC07	E	1,199	382	122	5	Transpo T41	None

1. Tensile bond strength only for the successful tests (shaded rows). For all other rows values in this column are the "lower bounds" for the tensile bond strength.
2. Failure comprising all three types (1, 2 and 3) of failure at the same time
3. Inclined holes filled with glue ensured increased bonded area and additional load transfer via bearing.
4. Failed at the head of the embedded bolt – not considered a successful pull-out test.



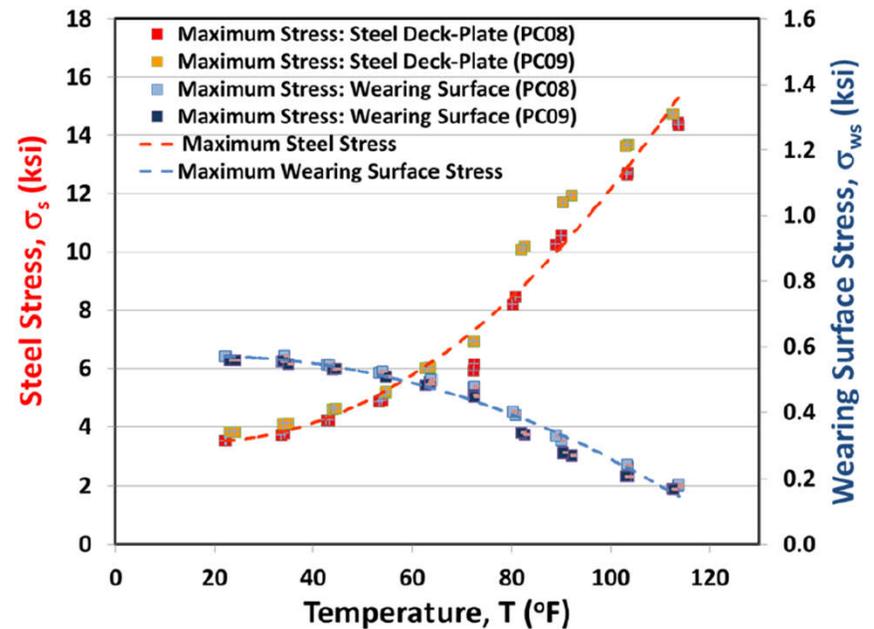
PPC FOR ORTHOTROPIC STEEL DECKS

SAN MATEO HAYWARD BRIDGE – EFFECTS OF TEMPERATURE



Steel and wearing surface stress as a function of wearing surface temperature (from EA composite specimens evaluated at the maximum load of 1,350 lbs.).

- Epoxy Asphalt Concrete (EAC)



Steel and wearing surface stress as a function of wearing surface temperature (from PC composite specimens evaluated at the maximum load of 1,350 lbs.).

- Polyester Polymer Concrete (PPC)



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PPC FOR ORTHOTROPIC STEEL DECKS

ROWAN UNIVERSITY → EAC VS PPC VS ROSPHALT

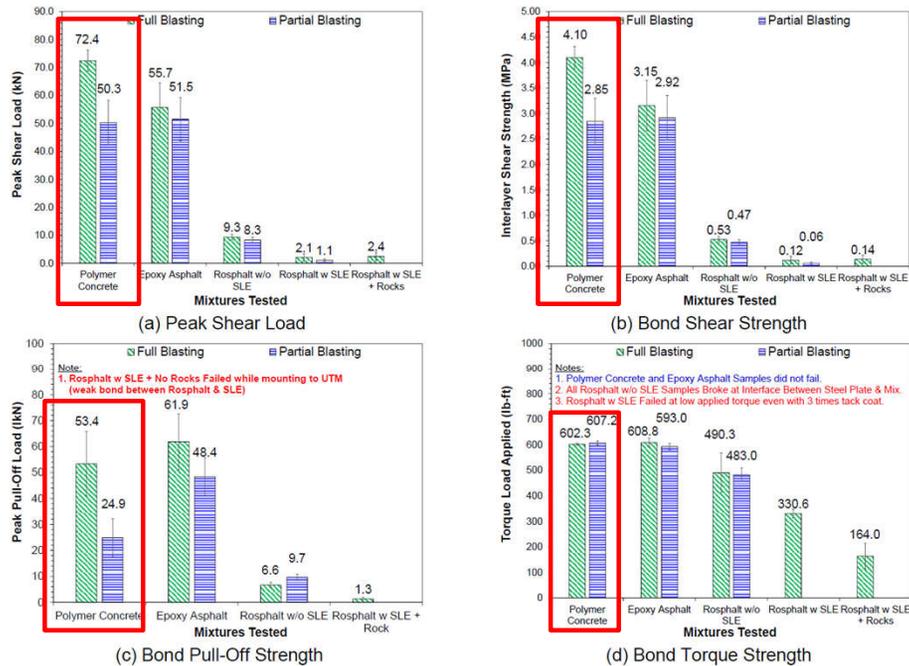


Figure 8. Shear, Pull-Off, and Torque Bond Strength Results.

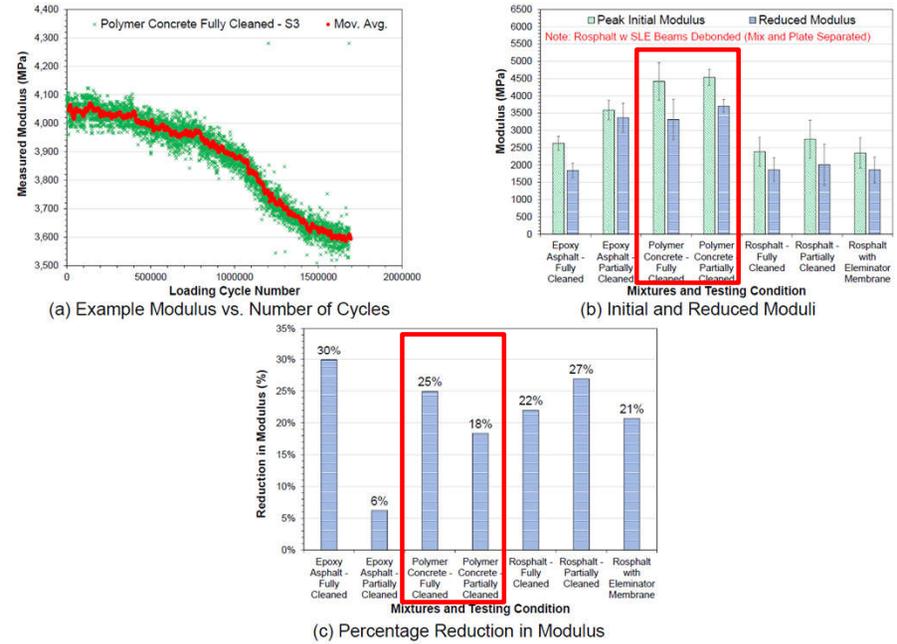


Figure 9. Cyclic Beam Fatigue Testing Results.

PPC FOR ORTHOTROPIC STEEL DECKS

ROWAN UNIVERSITY → EAC VS PPC VS ROSPHALT

SHEAR, PULL-OFF & TORQUE BOND STRENGTH

- PPC was better than EAC in test (a) Peak Shear Load by 30%
- PPC was better than EAC in test (b) Bond Shear Strength by 30%
- PPC was tied to EAC in test (d) Bond Torque Strength (only due to maxing the device)
- PPC was worse than EAC in test (c) Bond Pull-off test by only 13%
 - (However, test results from UofMC report for Caltrans San Mateo shows PPC having 60% higher pull strength than EAC)

CYCLIC LOAD FATIGUE TESTING

- PPC had an 81% higher elastic modulus than EAC on fully cleaned substrate
 - *30% reduction of EAC/Clean x 2600 MPa = 1820 MPa*
 - *25% reduction of PPC/Clean x 4400 MPa = 3300 MPa → **81% higher than EAC/Clean!***
- PPC had an 69% higher elastic modulus than EAC on partially cleaned substrate
 - *6% reduction of EAC/Partial x 1700 MPa = 1598 MPa*
 - *18% reduction of PPC/Partial x 3300 MPa = 2706 MPa → **69% higher than EAC/Partial!***



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PPC FOR ORTHOTROPIC STEEL DECKS

EXAMPLES OF PPC WEARING SURFACES ON OSD

- San Mateo Hayward Bridge (2015)
 - 2.5" thick x 450,000 SF
 - Installed in 2015 during 2 each 55-hour weekend closures
- Poplar Street Bridge (2012 / Trial)
- Yukon River Bridge (2013 / Trial)
- Ben Franklin Bridge (2022 / Trial)
- Danziger Bridge (2019 and beyond, routine patching and repair)
- 680 in Alameda County (2023)
 - 3.5 to 5" thick in California

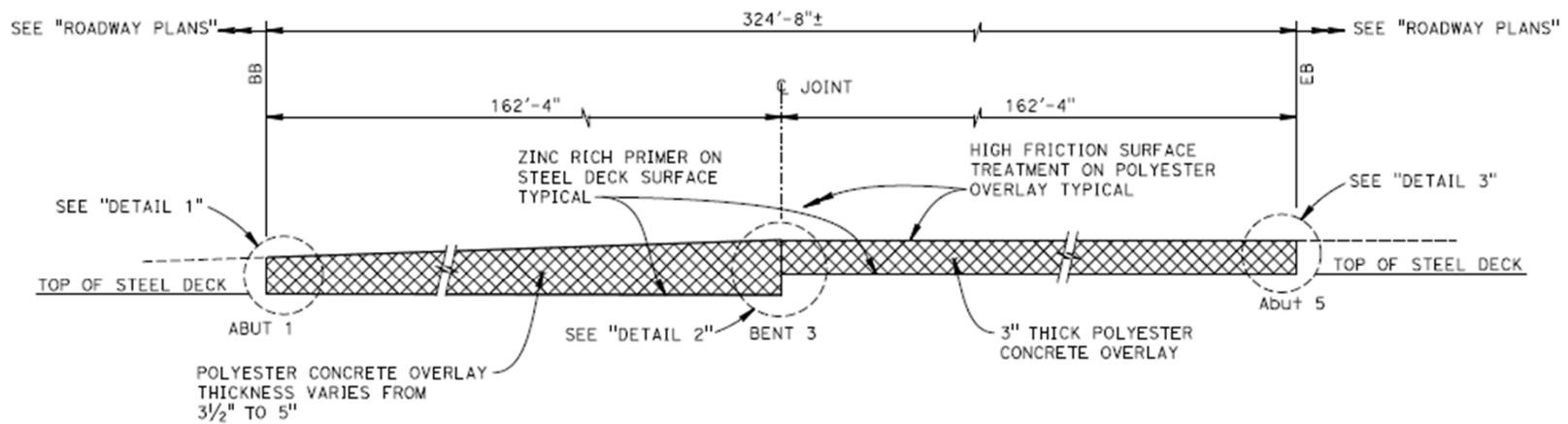


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PPC FOR ORTHOTROPIC STEEL DECKS

EXAMPLES OF PPC WEARING SURFACES ON OSD



LONGITUDINAL SECTION
NO SCALE

NOTE:

For details 1, 2 & 3, see "DECK OVERLAY DETAIL 2" sheet.

REMOVE EXISTING AS
CONCRETE AND PLAC
POLYESTER CONCRET

680 in Alameda, CA (2023)

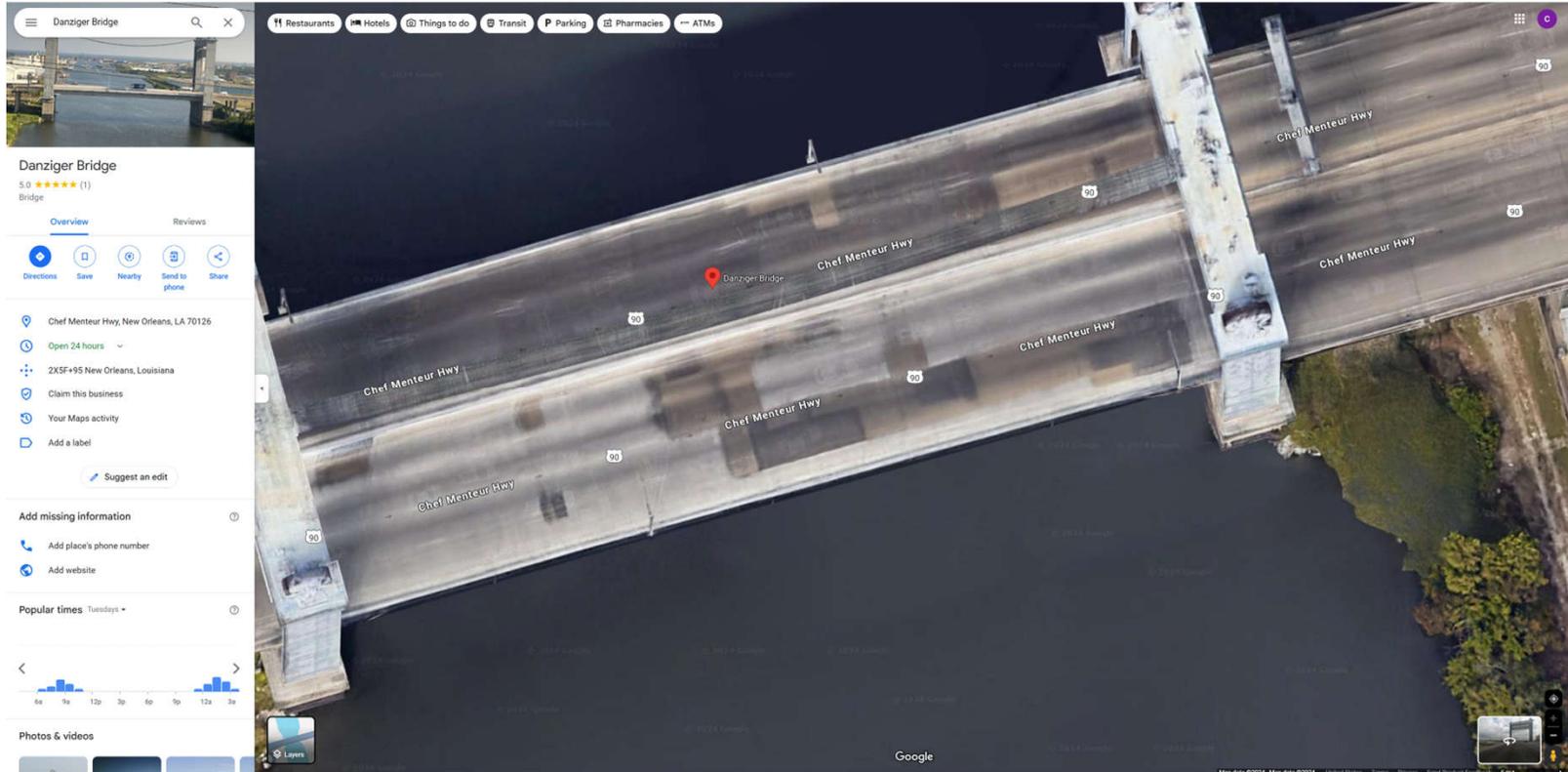


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PPC FOR ORTHOTROPIC STEEL DECKS

EXAMPLES OF PPC WEARING SURFACES ON OSD



Danziger Bridge, LA (2019)



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Casey Rafter
VP Sales
Kwik Bond Polymers, a Sika Company
(703) 881-8883
rafter.casey@us.sika.com



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